#### Committee of Experts on the Transport of Dangerous Goods and on the Globally Harmonized System of Classification and Labelling of Chemicals

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Sub-Committee of Experts on the Transport of Dangerous Goods

**Fifty-eighth session** Geneva, 28 June-2 July 2021 Item 6 (c) of the provisional agenda **Miscellaneous proposals for amendments to the Model Regulations on the Transport of Dangerous Goods: portable tanks** 

> Inclusion of the new section 6.9.3 "Requirements for design, construction, inspection and testing of fibre reinforced plastic (FRP) valves, relief devices and manholes for portable tanks"

Submitted by the Russian Federation

Committee of Experts on the Transport of Dangerous Goods and on the Globally Harmonized System of Classification and Labelling of Chemicals Sub-Committee of Experts on the Transport of Dangerous Goods Fifty-eighth session Geneva, 28 June - 02 July 2021

# Environmental effects onto mechanical properties of FRP materials for valves, relief devices and manholes of portable tanks

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Center for Design Manufacturing and Materials

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## Why FRP?



## Disadvantages of the steel valves, relief devices and manholes: low corrosion resistance when exposed to aggressive substances

Advantages of the FRP valves, relief devices and manholes: high strength-to-density ratio & corrosion resistance





# Why FRP?

#### FRP vs. steel equipment

	Manhole D500	Safety valve D80	Butterfly valve D80	Air line ball valve D32
FRP, kg	6	3,6	3	1,4
Typical steel, kg	17	7,1	6	2,9

### Structural performance of the FRP equipment

Service temperature, °C	-60+60
Maximum allowable working pressure, MPa	2,5
Attachment	Flanged / Coupling
Service fatigue life, cycles / years	6000 / 10
Hydraulic resistance	< 0,5

### **FRP examples**

1000P	70% polyphenylene sulfide resin / 30% E-glass D 7-10 mm, L 50 mm / additives 10%	Injection molding
G	40% modified phenol-formaldehyde resin / 60% E-glass D 16 mm, L 50 mm	Press molding
DSV	70% polyphenylene sulfide resin / 30% E-glass D 7-10 mm, L 6 mm / additives 10%	Injection molding



## **Environmental effects**

Corrosive air phase	Mechanical
service temperature	Corrosi
	substances

## Test program

#	Exposure	Mechanical
		tests
1	+20°C	ISO 527-4
2	+60°C	ISO 527-4
3	-60°C	ISO 527-4
4	+20°C, 168 hours of UV	ISO 527-4
5	+35°C / 168 hours of salt fog, ISO 12944-2, ISO 12944-6	ISO 527-4
6	+20°C, 168 hours of NaOH 40%(UN 1824), ISO 175	ISO 527-4
7	+20°C, 168 hours of H <sub>2</sub> SO <sub>4</sub> 95% (UN 1830), ISO 175	ISO 527-4
8	+20°C, 168 hours of HCl 37% (UN 1789), ISO 175	ISO 527-4
9	+20°C	ISO 13003, fatigue



## Tensile strength







## Elasticity modulus







## Fatigue



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 $K = K_0 \times K_1 \times K_2 \times K_3 \times K_4 \times K_5$ 

 $K_0$  is a strength factor = 1.5

 $K_1$  is a factor related to the deterioration in the material properties due to effects of chemicals

 $K_2$  is a factor related to the service temperature and the thermal properties

 $K_3$  is a factor related to the fatigue of the material

 $K_4$  is a factor related to the deterioration in the material properties due to effects of salt fog

 $K_5$  is a factor related to the deterioration in the material properties due to effects of UV exposure



$$K = K_0 \times \mathbf{K}_1 \times K_2 \times K_3 \times K_4 \times K_5$$

 $K_{\mathbf{1}}\;$  is a factor related to the deterioration in the material properties due to effects of chemicals

$$K_1 = \frac{\sigma_n}{\sigma_{eff}}$$

 $\sigma_n$  – nominal tensile strength

 $\sigma_{eff}$  – tensile strength after chemical exposure

 $\sigma_{eff} = \min(\sigma_{eff}^1, \sigma_{eff}^2, \dots, \sigma_{eff}^k), 1, 2, \dots, k$  - substance identifiers

	1000P	G	DSV
H <sub>2</sub> SO <sub>4</sub>	1.25	Dissolution	1.78
HCI	1.07	2.94	1.43
NaOH	1.06	1.80	1.42
K <sub>1</sub>	1.25	8	1.78

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$$K = K_0 \times K_1 \times \mathbf{K}_2 \times K_3 \times K_4 \times K_5$$

 $K_2$  is a factor related to the service temperature and the thermal properties

 $K_2 = \frac{\sigma_n}{\sigma_{temp}}$ 

- $\sigma_n$  nominal tensile strength
- $\sigma_{temp}$  tensile strength under working temperature

 $\sigma_{temp} = \min(\sigma_{temp}^1, \sigma_{temp}^2, \dots, \sigma_{temp}^k)$ , 1,2...,k-temperature identifiers

	1000P	G	DSV
- 60 <sup>0</sup> C	0.88	1.29	0.83
+ 60 <sup>0</sup> C	1.06	1.82	1.18
<i>K</i> <sub>2</sub>	1.06	1.82	1.18

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$$K = K_0 \times K_1 \times K_2 \times \mathbf{K}_3 \times K_4 \times K_5$$

 $K_3$  is a factor related to the fatigue of the material

 $K_3 = \frac{\sigma_n}{\sigma_N}$ 

 $\sigma_n$  – nominal tensile strength

 $\sigma_N$  – failure stresses for a given number of loading cycles

	1000P	G	DSV
$\sigma_n$	105.7	32.3	106
$\sigma_{N=10000}$	68.7	17.8	58.3
<b>K</b> <sub>3</sub>	1.54	1.82	1.82

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$$K = K_0 \times K_1 \times K_2 \times K_3 \times \mathbf{K_4} \times K_5$$

 $K_4$  is a factor related to the deterioration in the material properties due to effects of salt fog

$$K_4 = \frac{\sigma_n}{\sigma_{sf}}$$

 $\sigma_n$  – nominal tensile strength

 $\sigma_{sf}$  – tensile strength after salt fog exposure

	1000P	G	DSV
$\sigma_n$	105.7	32.3	106
$\sigma_{sf}$	94.3	16.1	54.8
<b>K</b> <sub>4</sub>	1.12	2.01	1.93



$$K = K_0 \times K_1 \times K_2 \times K_3 \times K_4 \times \mathbf{K_5}$$

 $K_5$  is a factor related to the deterioration in the material properties due to effects of UV exposure

 $K_5 = \frac{\sigma_n}{\sigma_{UV}}$ 

 $\sigma_n$  – nominal tensile strength

 $\sigma_{UV}$  – tensile strength after UV exposure

	1000P	G	DSV
$\sigma_n$	105.7	32.3	106
$\sigma_{UV}$	99.5	16.6	83.5
<b>K</b> <sub>5</sub>	1.06	1.95	1.27

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 $K = K_0 \times K_1 \times K_2 \times K_3 \times K_4 \times K_5$ 

	1000P	G	DSV
K <sub>0</sub>	1.5	1.5	1.5
<i>K</i> <sub>1</sub>	1.25	8	1.78
<i>K</i> <sub>2</sub>	1.06	1.82	1.18
<i>K</i> 3	1.54	1.82	1.82
<i>K</i> 4	1.12	2.01	1.93
<i>K</i> <sub>5</sub>	1.06	1.95	1.27
K	3.64	8	13.97

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# Thank you for your time!

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