# Development of a World-wide Worldwide harmonized Light duty driving Test Cycle (WLTC) 

## ~ Draft Technical Report ~

## UN/ECE/WP.29/GRPE/WLTP-IG <br> DHC subgroup

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## 1. Introduction

The development of the WLTC was carried out under a program launched by the World Forum for the Harmonization of Vehicle Regulations (WP.29) of the United Nations Economic Commission for Europe (UN-ECE) through the working party on pollution and energy transport program (GRPE). The aim of this project was to develop a World-wide harmonized Light duty driving Test Cycle (WLTC), to represent typical driving characteristics around the world, to have of a legislative worldwide harmonized type approval procedure put in place from 2014 onwards.

Driving cycles are produced by different countries and organizations and used to assess the performance of vehicles, such as pollutant emissions, fuel consumption and traffic impact. There are two main categories of test cycles: legislative cycles employed in type-approval tests for vehicles emissions certification and non-legislative cycles mainly used in research. Several international harmonized engine dynamometer cycles have been developed for engine emission certification of heavy-duty and non-road engines (WHSC, WHTC, NRTC). A worldwide harmonized test cycle has been developed also for motorcycles emissions (WMTC).

For Light-Duty (LD) vehicles, various vehicle dynamometer test cycles are employed in type-approval tests for emission certification. Such test cycles are: the NEDC ${ }^{1}$ used in Europe, JC08 ${ }^{2}$ applied in Japan, the UDDS (FTP-75) ${ }^{3}$ used in the United States. The NEDC cycle includes four urban driving cycle (ECE) segments characterized by low vehicle speed, low engine load, and low exhaust gas temperature, followed by one extra-urban segment to account for more aggressive and higher speed driving. JC08, represents driving in congested city traffic, including idling periods and frequently alternating acceleration and deceleration. In the U.S, currently the Federal Test Procedure (FTP-75) is used for emission certification of cars and light duty trucks. The US FTP - 75 is a transient cycle produced from real measurements in Los Angeles and it represents only a specific region in the US.

Each of these driving cycles has advantages and drawbacks/disadvantages. For example, NEDC, which consists of several steady-steady test modes, is quite simple to drive and thus repeatable. However, it is well known that NEDC does not represent real driving behavior of a vehicle in actual traffic thus, does not accurately reflect pollutant emissions and fuel consumption. JC08 represents real driving behavior but only in congested city traffic situations and does not cover other driving conditions and road types. FTP-75 covers a wider range of driving conditions than JC08, however it is still not complete enough to cover all possible driving situations (in fact, in the USA, vehicles have to be additionally tested on two Supplemental Federal Test Procedures (SFTP) designed to address shortcomings with the FTP-75 in the representation of (1) aggressive, high speed driving (US06), and (2) the use of air conditioning (SC03)).

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Therefore, when the WLTC project was started it was agreed to design a new legislative driving cycle to predict more accurately the exhaust emissions and fuel consumption under real-world driving conditions.

The world-wide harmonized light duty test cycle (WLTC) presented in this paper, was derived from "real world" driving data from five different regions: EU + Switzerland, USA, India, Korea and Japan covering a wide range of vehicle categories (M1, N1 and M2 vehicles, various engine capacities, power-to-mass ratios, manufacturers etc), over different road types (urban, rural, motorway) and driving conditions (peak, off-peak, weekend).

## 2. Objective

The objectives of the Development of the worldwide Harmonized test Cycle (DHC) group under the WLTP informal group are to develop a world-wide harmonized light duty driving test cycle (WLTC) which represents typical driving characteristics around the world and to develop a gearshift procedure which simulates representative gearshift operation for light duty vehicle.

## 3. Structure of the project

The development of the cycle and the gearshift procedure belong to the tasks of the WLTP Informal Group (WLTP-IG). The three groups were established under the WLTP informal group in order to allocate important elements to each. Figure 3-1 shows the structure of WLTP-IG.

- The Development of the worldwide Harmonized test Cycle (DHC) group aims to develop the WLTC
- The Development of Test Procedure (DTP) group aims to develop the test procedure
- The Validation Task Force team aims to manage the validation test phase 2


Figure 3-1 The structure of WLTP-IG

Figure 3-2 shows the overview of the WLTC development.
In the work schedule of the WLTP-IG, the two validation steps were conducted after the development of the initial test cycle and gearshift procedure. As the first step, the drivability and traceability was evaluated in the validation test phase 1. As the second step, the emission measurement results based on the proposed test procedure input from DTP group were evaluated.

Figure 3-3 shows the time schedule for Cycle development. The development of WLTC has started since September 2009.

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Figure 3-2 Overview of the WLTC development


Figure 3-3 The time schedule for Cycle development

## 4. Cycle development

### 4.1. Approach

Driving behaviors data and weighting factor matrix based on statistical information about light duty vehicle use in the different regions of the world were collected and analyzed as fundamentals to develop the cycle. The in-use driving behaviors data were combined with the statistical information on vehicle use in order to develop a reference database that is represents worldwide light duty vehicle driving behaviors. Figure 4-1 shows the overview of the cycle development process Real world in-use data was collected from a range of Contracting Parties in the following regions:
$\cdot$ EU and Switzerland,

- India,
- Japan,
- Korea,
- USA,

Then, a reference database was developed. In-use data were weighted and aggregated to produce unified speed-acceleration distributions. Analysis was undertaken to determine the average short trip durations and idling times which were used to determine the number of short trips that should be included in each drive cycle phase.

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Short trips were combined to develop the final drive cycle
The short trip combination and the reference database were compared on the basis of the chi-squared method for the speed -acceleration distribution. The combination of short trips with the least chi-squared value was selected as the ideal combination. After the short trip selection, the comparison of the other parameters such as average speed, Relative Positive Acceleration (RPA) etc. was conducted to check the representativeness.

Finally a first draft of the WLTC was produced. The first draft had been expected to need modifying based on some evaluations of validation tests.


Figure 4-1 Overview of the cycle development process

### 4.2. In-use driving behavior data

The in-use data collection guidelines ${ }^{4}$ were developed and agreed following a full discussion at the 1 st DHC meeting held in September 2009. The each contracting party has started to gather the in-use data from January 2010.

The in-use driving data (second by second recording of time, vehicle speed, engine speed, GPS - Global Positioning System - information, in some cases also: altitude, engine load, accelerometer) used for the development of the WLTC was collected from five different regions: European Union (EU) + Switzerland (CH), USA (US), Japan (JP), Korea (KR), and India (IN). Within EU, collection campaigns have been organized in Germany (DE), Spain (ES), Italy (IT), Poland (PL), Slovenia (SI), United Kingdom (UK), Belgium (BE), France (FR) and Sweden (SE). Over 765, 000 km of data was collected covering a range of vehicle categories (M1, N1

[^1]and M2 vehicles, various engine capacities, power-to-mass ratios, manufacturers etc), over different road types (urban, rural, motorway) and driving conditions (peak, off-peak, weekend).

Table 4-1 summarizes the vehicle type, number of vehicles, total mileage for each region and the methodology used to collect the available in-use driving behavior data. India, Japan and Korea used "instructed drivers" (Drivers were instructed to follow the traffic flow), $\mathrm{EU}+\mathrm{CH}$ collected data from "customer data" (drivers without any particular instruction to drive their cars). India submitted both "customer data" and "instructed drivers data". Finally, USA submitted both "customer data" and instructed drivers using the "chase car" method. The chase cars were equipped with laser rangefinders mounted behind the front grill to measure the vehicle speed of randomly selected vehicles.

Table 4-1 Total amount of data collection (Available data)

| Region/Country |  | $\begin{gathered} \text { Vehicle type } \\ \hline \text { PC } \end{gathered}$ | No. of vehicles <br> 12 | Method used for collection | Total amount of data collection (km) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{EU}+\mathrm{CH}$ | Belgium (BE) |  |  | Customer data | 106,952 | 106,952 |
|  |  | LDCV | 0 |  | 0 |  |
|  | Germany (DE) | PC | 8 |  | 23,414 | 23,414 |
|  |  | LDCV | 0 |  | 0 |  |
|  | Spain (ES) | PC | 6 |  | 2,619 | 9,666 |
|  |  | LDCV | 4 |  | 7,047 |  |
|  | France (FR) | PC | 42 |  | 108,916 | 108,916 |
|  |  | LDCV | 0 |  | 0 |  |
|  | Italy (IT) | PC | 8 |  | 57,646 | 57,646 |
|  |  | LDCV | 0 |  | 0 |  |
|  | Poland (PL) | PC | 9 |  | 14,648 | 14,648 |
|  |  | LDCV | 0 |  | 0 |  |
|  | Slovenia (SI) | PC | 18 |  | 48,934 | 48,934 |
|  |  | LDCV | 0 |  | 0 |  |
|  | Switzerland (CH) | PC | 26 |  | 22,670 | 23,619 |
|  |  | LDCV | 4 |  | 949 |  |
|  | United Kingdom (UK) | PC | 10 |  | 17,491 | 31,781 |
|  |  | LDCV | 12 |  | 14,290 |  |
|  | Sweden (SE) | PC | 5 |  | 18,525 | 36,951 |
|  |  | LDCV | 2 |  | 18,426 |  |
| India (IN) |  | PC | 16 | Instructed drivers and Customer data | 41,804 | 55,778 |
|  |  | LDCV | 4 |  | 13,974 |  |
| Japan (JP) |  | PC | 11 | Instructed drivers | 25,670 | 52,955 |
|  |  | LDCV | 13 |  | 27,285 |  |
| Korea (KR) |  | PC | 6 | Instructed drivers | 26,033 | 34,403 |
|  |  | LDCV | 2 |  | 8,370 |  |
| USA (US) |  | PC | 156 | Instructed drivers and Customer data | 130,188 | 159,726 |
|  |  | LDCV | 20 |  |  |  |
|  |  | unclear | - | Chased car | 29,538 |  |

### 4.3. Data Analysis Processing

The processing of the raw data involved initially filtering and thinning the in-use driving behavior data. Filtering was performed using a standard smoothing algorithm (T4253H) as described in the SPSS software ${ }^{5}$ Reducing data frequency from 10 Hz to 1 Hz was necessary only for a limited amount of data as most of the data was 1 Hz data. The resulting smoothed data was converted into idling and short trips portions to create short trips and idles databases for each region/country and for each part of the cycle (e.g: urban, rural, motorway phases). A series of elimination criteria have been applied to the short trip and idle databases for determining the short trips and idle periods to be excluded from the subsequent analysis (e.g. idling periods with duration higher than ten minutes, short trips with duration smaller than ten seconds, short trips with the maximum speed less than $3.6 \mathrm{~km} / \mathrm{h}$, short trips with accelerations higher than $4 \mathrm{~m} / \mathrm{s}^{2}$ and smaller than $-4.5 \mathrm{~m} / \mathrm{s}^{2}$ etc). The short trip and idle databases so obtained were used to determine: short trip duration cumulative frequency distributions, short trip average speed distribution, idling duration distribution which were furthermore used for developing the unified distributions.

[^2]

Figure 4-2 Data Analysis Processing

### 4.4. The development of the world-wide harmonized light duty test cycle (WLTC)

The methodology to develop the WLTC ${ }^{6}$ was reviewed and agreed following a full discussion at the 2nd DHC meeting held in January 2010. Then the revised methodology ${ }^{7}$ proposed by Japan was agreed at the 6th DHC meeting.

### 4.4.1. Re-categorization of In-use driving data

During data analysis, it became soon evident that the road category (urban, rural, motorway) could not be used due to differences in definitions and speed limits of these road categories from different regions. (Table 4-2)

[^3]Table 4-2 Definition of Road Type in each region

|  | Urban | Rural | Motorway |
| :---: | :---: | :---: | :---: |
| India | Paved roads in urban areas with a speed limit $\leq 40$ km/hour (exclude mountain areas) | Paved non-motorways outside and inside urban areas with a speed limit between 40 and 60 km/hour | Paved motorways (multi-lane roads specifically constructed and controlled for fast traffic) with a speed 60 to $\mathbf{8 0} \mathbf{~ k m} /$ hour |
| Korea | Arterial, collector and local road inside and/or near central business district (CBD). Speed limit is from 40 to $\mathbf{8 0} \mathbf{~ k m} / \mathrm{h}$, depends on road type | Arterial, collector and local road inside non-urban area. Speed limit is from 50 to $80 \mathbf{~ k m} / \mathrm{h}$, depends on road type | Motorway which is designed, constructed and controlled for faster traffic in urban and rural area. Speed limit is from 100 to 120 km/h, depends on area |
| Japan | Densely Inhabited District (DID) <br> - Speed limit $\leq 60 \mathrm{~km} / \mathrm{h}$ <br> - exclude mountain areas | - Non-Densely Inhabited District <br> - Non motorways <br> - Speed limit $\leq 60 \mathrm{~km} / \mathrm{h}$ <br> - exclude mountain areas | Motorways <br> (within City and between Cities) <br> - Speed limit $\leq 100 \mathrm{~km} / \mathrm{h}$ <br> - exclude mountain areas |
| EU | The definition depends on EU countries | The definition depends on EU countries | The definition depends on EU countries |

Figure 4-3 shows the vehicle speed cumulative frequency distribution of various countries on urban, rural and motorway road types.


Figure 4-3 Vehicle speed cumulative frequency distribution of various countries on urban, rural and motorway roads

While for the urban road type there was encouraging evidence that all in-use driving behavior data can concur, for the rural and motorway road categories there was a clear difference between Europe on the one hand and Japan + Korea on the other hand. Figure 2 shows the speed cumulative frequency distribution for Japan and Korea almost $100 \%$ at vehicle speed of $80 \mathrm{~km} / \mathrm{h}$ while for all European countries the $100 \%$ speed cumulative frequency distribution is reached at vehicle speed $>100 \mathrm{~km} / \mathrm{h}$. On motorways roads (figure 3) this difference is even higher.

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Korea and Japan have motorway top speed of $100 \mathrm{~km} / \mathrm{h}$ while in Europe the top speed is between $120-140 \mathrm{~km} / \mathrm{h}$. This was further confirmed when the Indian and USA in-use driving behavior data were added to the world-wide database. Therefore, it became necessary to develop the WLTC cycle on speed classes (low, medium and high speed) rather than on road categories (urban, rural, motorway). Furthermore the high speed phase was split in two segments: one high speed phase with a top speed value representative of Asian driving and one extra-high speed phase with a top speed more characteristic to the European and USA driving. Eventually, the world-wide harmonized test cycle (WLTC) consists of four speed phases (low, medium, high and ex-high). Having decided to develop the WLTC in four phases, a crucial aspect was to establish the speed limit between the four phases. The threshold vehicle speed between the Low/Medium/High and Extra High phases, was chosen after a comparative study for different candidate criteria (low speed $<50 \mathrm{~km} / \mathrm{h} /$ medium speed $<70 \mathrm{~km} / \mathrm{h} /$ high speed $<110 \mathrm{~km} / \mathrm{h}$ / ex-high > $110 \mathrm{~km} / \mathrm{h}]$; [50/80/110]; [50/80/120]; [50/90/110]; [50/90/120]; [60/80/110]; [60/80/120]; [60/90/110]; [60/90/120]; [70/90/110]; [70/90/120]; [70/100/120]) was performed. Figure $4-4$ and Figure $4-5$ present the speed-acceleration distributions for each region for some of the above mentioned combinations. As can be seen, the best compromise in terms of similarity of speed-acceleration distribution of each region and the unified values of the parameters (average speed, short trip duration distribution, idle duration distribution) could be obtained with threshold speed values of $60 / 80 / 110$ between the phases.

| U/R/M | Urban | Rural | Motorway |
| :---: | :---: | :---: | :---: |
| EU |  |  |  |
| India |  |  |  |
| Japan |  |  |  |
| Korea |  |  |  |
| US |  |  |  |

Figure 4-4 Speed-acceleration distribution in U/R/M category


Figure 4-5 Speed-acceleration distribution in L/M/H/ExH category [60/80/110]

### 4.4.2. Statistics and Regional weighting factor

The driving cycle was developed from recorded in-use data ("real world" data) from different regions of the world (EU, India, Japan, Korea, USA) combined with suitable weighting factors. Regional weighting for L/M/H/Ex-H phases was necessary to represent each region driving characteristics when developing the unified distributions and harmonized cycle. The weighing factors were based on traffic volumes (current and foreseen) of each party. To derive such weighing factors the starting point was the national traffic statistics ${ }^{8}$ (as shown in Table 4-3).

[^4]Table 4-3 Traffic volume (vehicle hours)

| Region |  | Traffic volume (vehicle hours) |  |  |  | Traffic volume ratio (\%) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Urban | Rural | Motorway | Total | Urban | Rural | Motorway | Total |
| Worldwide | EU | 3.30E+10 | 3.02E+10 | 4.73E+09 | $6.79 \mathrm{E}+10$ | 48.5 | 44.5 | 7.0 | 100.0 |
|  | US | $4.95 \mathrm{E}+10$ | $2.01 \mathrm{E}+10$ | $1.97 \mathrm{E}+10$ | $8.93 \mathrm{E}+10$ | 55.4 | 22.5 | 22.1 | 100.0 |
|  | JP | $1.10 \mathrm{E}+10$ | $6.46 \mathrm{E}+09$ | $1.30 \mathrm{E}+09$ | $1.88 \mathrm{E}+10$ | 58.7 | 34.4 | 6.9 | 100.0 |
|  | KR | $4.26 \mathrm{E}+09$ | 1.51E+09 | $2.64 \mathrm{E}+09$ | $8.42 \mathrm{E}+09$ | 50.6 | 18.0 | 31.4 | 100.0 |
|  | IN | $2.10 \mathrm{E}+10$ | 7.22E+09 | $1.53 \mathrm{E}+09$ | $2.98 \mathrm{E}+10$ | 70.6 | 24.2 | 5.1 | 100.0 |
|  | Total | $1.19 \mathrm{E}+11$ | $6.55 \mathrm{E}+10$ | $2.99 \mathrm{E}+10$ | $2.14 \mathrm{E}+11$ | 55.4 | 30.6 | 14.0 | 100.0 |
| $\mathrm{EU}+\mathrm{CH}$ | BE | $5.46 \mathrm{E}+08$ | 1.02E+09 | $2.39 \mathrm{E}+08$ | 1.80E+09 | 30.3 | 56.4 | 13.3 | 100.0 |
|  | DE | $5.83 \mathrm{E}+09$ | 4.24E+09 | $1.12 \mathrm{E}+09$ | $1.12 \mathrm{E}+10$ | 52.1 | 37.9 | 10.0 | 100.0 |
|  | ES | $4.51 \mathrm{E}+09$ | 3.71E+09 | $2.83 \mathrm{E}+08$ | 8.51E+09 | 53.1 | 43.6 | 3.3 | 100.0 |
|  | FR | $5.35 \mathrm{E}+09$ | 5.37E+09 | $8.59 \mathrm{E}+08$ | $1.16 \mathrm{E}+10$ | 46.2 | 46.4 | 7.4 | 100.0 |
|  | IT | $2.19 \mathrm{E}+09$ | 3.23E+09 | $6.13 \mathrm{E}+08$ | $6.03 \mathrm{E}+09$ | 36.3 | 53.5 | 10.2 | 100.0 |
|  | PL | $8.41 \mathrm{E}+08$ | $1.45 \mathrm{E}+09$ | $3.23 \mathrm{E}+07$ | $2.33 \mathrm{E}+09$ | 36.1 | 62.5 | 1.4 | 100.0 |
|  | SI | $1.23 \mathrm{E}+08$ | 7.55E+07 | $1.89 \mathrm{E}+07$ | $2.18 \mathrm{E}+08$ | 56.7 | 34.7 | 8.7 | 100.0 |
|  | UK | 7.07E+09 | 3.83E+09 | $5.31 \mathrm{E}+08$ | 1.14E+10 | 61.8 | 33.5 | 4.6 | 100.0 |
|  | CH | 7.23E+08 | 1.05E+09 | 1.97E+08 | 1.97E+09 | 36.7 | 53.3 | 10.0 | 100.0 |
|  | SE | - | - | - | $1.31 \mathrm{E}+09$ | - | - | - | 100.0 |

After subdividing the database of each party into these four speed phases, the time percentage of each of them was multiplied by the total vehicle hour of the party, obtaining the vehicle hour for each speed class and each party (see Table 4-4). For India an exception was applied (total traffic volume increased by $50 \%$ in the light of the predicted increase over next years). From this, the weighing factors as shown in Figure 4-6 were defined.

Table 4-4 Traffic volume ratio between the L/M/H/ExH phase [million vehicle hours]

| Region | Traffic volume (vehicle hours) |  |  |  |  | Traffic volume ratio (\%) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Low | Middle | High | Ex-H | Total | Low | Middle | High | Ex-H | Total |
| EU+CH | $2.33 \mathrm{E}+10$ | 1.24E+10 | 1.57E+10 | $1.64 \mathrm{E}+10$ | $6.79 \mathrm{E}+10$ | 34.4 | 18.3 | 23.2 | 24.1 | 100.0 |
| US | $1.59 \mathrm{E}+10$ | $2.26 \mathrm{E}+10$ | 2.95E+10 | $2.13 \mathrm{E}+10$ | $8.93 \mathrm{E}+10$ | 17.8 | 25.3 | 33.1 | 23.8 | 100.0 |
| JP | 1.11E+10 | 6.16E+09 | 1.16E+09 | $3.28 \mathrm{E}+08$ | $1.88 \mathrm{E}+10$ | 59.3 | 32.8 | 6.2 | 1.7 | 100.0 |
| KR | $4.05 \mathrm{E}+09$ | 1.84E+09 | 2.09E+09 | $4.43 \mathrm{E}+08$ | 8.42E+09 | 48.1 | 21.8 | 24.8 | 5.3 | 100.0 |
| IN | $1.56 \mathrm{E}+10$ | 8.47E+09 | $5.64 \mathrm{E}+09$ | $6.42 \mathrm{E}+07$ | $2.98 \mathrm{E}+10$ | 52.4 | 28.4 | 18.9 | 0.2 | 100.0 |
| World-wide | $7.00 \mathrm{E}+10$ | $5.15 \mathrm{E}+10$ | $5.42 \mathrm{E}+10$ | $3.85 \mathrm{E}+10$ | $2.14 \mathrm{E}+11$ | 32.7 | 24.0 | 25.3 | 18.0 | 100.0 |



Figure 4-6 Regional weighting factors

To build the European database (which included the contribution of 9 EU member states + Switzerland) it was decided to use a slightly different approach. Starting from the observation/assumption that the driving behavior did not differ very much among EU countries, it was considered reasonable to give some weight also to the robustness of the single database. Thus, instead of considering only the traffic volume of the country (somewhat representative of the population) a $50 \%$ weight was assigned also to the mileage of each country's database. The result of this approach is shown in Figure 4-7.


Figure 4-7 Internal weighting factors for Europe

### 4.4.3. Determination of test cycle duration

The length of the world-wide harmonized test cycle was set to 1800 seconds similar to WHDC (World Harmonized Heavy Duty Cycle) and WMTC. This cycle duration represents an accepted compromise between statistical representativeness on the one hand and test feasibility in the laboratory on the other hand. The length of each speed phase (Low, Medium, High and Extra-high) was determined based on traffic volume ratio between the L/M/H/Ex-H phases (Low: 589 s, Mid.: 433 s, High: 455 s, Ex-High: 323 s) as shown in Table 4-5.

Table 4-5 The length of each speed phase

|  | (Unite: vehicle hours) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Low | Mid. | High | Ex-H | Total |
| EU | $2.33 \mathrm{E}+10$ | $1.24 \mathrm{E}+10$ | $1.57 \mathrm{E}+10$ | $1.64 \mathrm{E}+10$ | $6.79 \mathrm{E}+10$ |
| US | $1.59 \mathrm{E}+10$ | $2.26 \mathrm{E}+10$ | $2.95 \mathrm{E}+10$ | $2.13 \mathrm{E}+10$ | $8.93 \mathrm{E}+10$ |
| JP | $1.11 \mathrm{E}+10$ | $6.16 \mathrm{E}+09$ | $1.16 \mathrm{E}+09$ | $3.28 \mathrm{E}+08$ | $1.88 \mathrm{E}+10$ |
| KR | $4.05 \mathrm{E}+09$ | $1.84 \mathrm{E}+09$ | 2.09E+09 | $4.43 \mathrm{E}+08$ | $8.42 \mathrm{E}+09$ |
| IN | $1.56 \mathrm{E}+10$ | 8.47E+09 | $5.64 \mathrm{E}+09$ | $6.42 \mathrm{E}+07$ | $2.98 \mathrm{E}+10$ |
| World-wide | $7.00 \mathrm{E}+10$ | $5.15 \mathrm{E}+10$ | $5.42 \mathrm{E}+10$ | $3.85 \mathrm{E}+10$ | $2.14 \mathrm{E}+11$ |
| propotion | 0.327 | 0.240 | 0.253 | 0.180 | 1.000 |
|  |  |  |  |  |  |
| Cycle duration | 589 | 433 | 455 | 323 | 1800 |

### 4.4.4. Driving characteristics

Figure 4-8 - Figure 4-11 show the driving characteristics (average speed, RPA - Relative Positive Acceleration, average short trips duration and average idle duration) for each region (Japan, Europe, United States, Korea, India) and for the world-wide (unified) database.


Figure 4-8 RPA - driving characteristics

The Relative Positive Acceleration (RPA) is an important parameter to characterize vehicle trips and compare the load of the test cycle. It is a speed-related average of acceleration of the vehicle (power of a vehicle) calculated with the following equation: ${ }^{9}$


With being the acceleration at time step i, (only $a_{i}>0(\mathrm{~m} / \mathrm{s} 2), v_{i}$ being the vehicle speed at time step i ( $\mathrm{m} / \mathrm{s}$ ) and being the total trip distance (m).
The vehicle acceleration was calculated from consecutive vehicle speed samples according to the following equation.

$$
\mathrm{a}_{\mathrm{i}}=\left[\frac{v_{i+1}-v_{i-1}}{2}\right] \div 3.6
$$

[^5]

Figure 4-9 Average speed - driving characteristics


Figure 4-10 Average idle duration - driving characteristics


Figure 4-11 Average short trip duration - driving characteristics

### 4.4.5. Determination of short trips and idles number

Having determined the length of each speed phase, the number of short trips and idle periods in each of them ( $\mathrm{L} / \mathrm{M} / \mathrm{H} / \mathrm{Ex}-\mathrm{H}$ ) was calculated according to equations 3-4. The resulting number was rounded to an integer number:

$$
\begin{equation*}
\mathrm{N}_{\mathrm{ST}, \mathrm{i}}=\frac{\text { phase duration }- \text { average idling duration }}{\text { average short trip duration }+ \text { average idling duration }} \tag{eq.3}
\end{equation*}
$$

$$
\mathrm{N}_{\mathrm{L}, \mathrm{i}}=\text { number of short trips }\left(\mathrm{N}_{\mathrm{sT}, \mathrm{i}}\right)+1
$$

Table 4-6 shows, for each speed phase ( $\mathrm{L} / \mathrm{M} / \mathrm{H} / \mathrm{Ex}-\mathrm{H}$ ), the total duration, the average short trip duration and average idle duration (as determined from data analysis and shown in Figure 4-10 and Figure 4-11), number of short trips and number of idles (as calculated according to Eqs.3-4).

Table 4-6 Determination of No. of ST and Idle for the L/M/H/ExH phases.

|  | Target cycle <br> duration | Average ST <br> duration | Average <br> IDLE <br> duration | No. of ST | No. of IDLE |
| :---: | ---: | :---: | :---: | :---: | ---: |
|  | s | s | s | $\#$ | $\#$ |
| Low | 589 | 84 | 22 | 5 | 6 |
| Middle | 433 | 238 | 22 | 1 | 2 |
| High | 455 | 446 | 23 | 1 | 2 |
| Extra-high | 323 | 824 | 14 | 1 | 2 |

Applying equation 3 , for the low and medium speed phase the number of short trips is higher than 1 , while for the high and extra-high speed phases equation 3 gives a number of short trips smaller than 1 (rounded to 1 ). This is due to the average short trip duration (as obtained from the unified database) being longer than the duration of the high and extra-high speed phase in the WLTC. To determine the duration of the short trips in one phase a cumulative frequency graph of the short trip duration had to be generated. Figure 4-12 shows the short trip length cumulative frequency distributions for determining the short trips duration in the low speed phase. The Y axis was divided into the five equally parts (five short trips calculated in the low speed phase) and by selecting the average duration in each part, the duration of the short trips (ST1, ST2, ST3, ST4, ST5) was decided. Similar procedure was applied for determining the idle periods duration.

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Figure 4-12 Cumulative frequency distributions of short trip duration.

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Figure 4-13 Number of ST and Idles and their duration for each phase of the WLTC

The short trips for WLTC had to be selected from the unified database. The selection criteria were based on the concept that the selected short trips must provide similar distributions of speed, acceleration, etc. to those of the unified database. Given the large number of different/possible short trips combinations, several selection criteria (average vehicle speed, acceleration duration ratio, deceleration duration ratio) were applied. This selection was necessary in order to reduce the number of possible combinations and to keep computation time for performing the chi-squared analysis to a reasonable limit. The combination of the short trips with the smallest chi-squared value was selected in the WLTC driving cycle.

### 4.4.6. The characteristics of first ST and Idling of the day

A separate statistical analysis has been performed in order to select the first short trip and the first idling of the driving cycle. Table $4-7$ summarizes the characteristics of this analysis (the average idle duration, average short trip duration, average speed, maximum speed). Based on these characteristics, from the five short trips part of the low speed phase, ST5's characteristics was the best fit with the first initial short trip of the day and therefore is the first short trip of the test cycle. The first idling of the test cycle with a duration of 28 seconds (from the six idles as shown in Figure 4-13) was considered to fit the most the characteristics of the first idle of the day.

- Average Idling duration of first Idling of a day is $28 \mathrm{~s} .=>$ Select 28 s
- The final Idling duration would be more than 5 s because of stable sampling. => Select 8 s
- Average speed of first short trip of a day is approx. $30 \mathrm{~km} / \mathrm{h}$. => ST of 245 s

Table 4-7 The characteristics of first ST and Idling of the day

| region | sample <br> number | stop <br> duration in <br> $\mathbf{s}$ | average <br> short trip <br> duration in <br> $\mathbf{s}$ | average <br> speed in <br> $\mathbf{k m / h}$ | maximum <br> $\mathbf{s p e e d}$ in <br> $\mathbf{k m / h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Europe | 3271 | 24.0 | 208.4 | 29.3 | 48.8 |
| USA | 1492 | 32.0 | 144.7 | 29.8 | 55.5 |
| Average | - | 28.0 | 176.5 | 29.6 | 52.2 |

### 4.4.7. The Extra-High Speed Phase

The selection of the Extra-high speed phase from the unified database was more challenging as/because the/its duration of 323 seconds (as determined by applying the methodology described earlier) was too small compared to the real world's extra-high short trips from the unified database. Therefore/for this reason, the extra-high speed phase was developed with a modified methodology based on a combination of different segments defined as: take-off, cruise and slow-down, extracted from real short trips from the unified database as shown in Figure 13b. The combination of the segments forming one extra-high short trip which fitted the most the characteristics (maximum speed, average speed, RPA, average positive acceleration, average speed $x$ positive acceleration) of a real extra-high short trip and with the smallest chi-squared value was selected to represent the extra-high speed phase in the WLTC driving cycle.

Candidate driving data


Figure 4-13b Image of the extra-high speed phase development methodology.
4.5. The initial world-wide harmonized light duty test cycle (WLTC version 1)

An initial WLTC was introduced by Japan in the 9th DHC meeting. Figure 4-14 shows the speed profile of the WLTC driving cycle. The first short trip in the driving cycle is the first short trip of the day as determined in Table 4-7 (average speed of first short trip of a day is approx. $30 \mathrm{~km} / \mathrm{h}$ ). The order of the other short trips in the low speed phase was set randomly. Also, the short trips with lowest speed were connected with the Idles with longest duration in order to reflect traffic jam. The speed acceleration distributions of WLTC ver. 1 were shown in Figure $4-15$. The characteristics of the WLTC driving cycle are shown in Table 4-8.


Figure 4-14 The speed profile of the WLTC driving cycle version 1.

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|  | Low | Midle |
| :---: | :---: | :---: |
| Unified distribution |  |  |
| WLTC ver. 1 |  |  |


|  | High | Ex-high |
| :---: | :---: | :---: |
| Unified distribution |  |  |
| WLTC ver. 1 |  |  |

Figure 4-15 The speed acceleration distribution of WLTC ver. 1

Table 4-8 The characteristics of the World-wide Light duty Test Cycle version 1 (WLTC ver.1)

| Parameter |  | Cycle <br> duration <br> $s$ | $\begin{gathered} \begin{array}{c} \text { Driving } \\ \text { distance } \end{array} \\ \hline \mathrm{km} \\ \hline \end{gathered}$ | Average speed <br> km/h | Max. <br> speed <br> km/h | Max. <br> acceleratio <br> $n$ <br> $\mathrm{~km} / \mathrm{h} / \mathrm{s}$ | Max. <br> Deceleratio <br> $n$ <br> $\mathrm{~km} / \mathrm{h} / \mathrm{s}$ | driving mode(*) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Acceleratio n ratio |  |  |  |  |  | $\begin{gathered} \text { Deceleratio } \\ \mathrm{n} \text { ratio } \end{gathered}$ | Cruise ratio | Idling ratio |
|  |  |  |  |  |  |  |  | \% | \% | \% | \% |
| Worldwide | Low |  |  |  | 19.8 | 60 | - | - | 27.5 | 25.4 | 22.7 | 24.5 |
|  | Middle | - | - | 38.4 | 80 | - | - | 31.4 | 27.5 | 28.8 | 12.2 |
|  | High | - | - | 58 | 110 | - | - | 31.3 | 27.2 | 35.5 | 6.0 |
|  | Extra-high | - |  | 86.8 | 194.7 | - |  | 25.7 | 23.4 | 48.9 | 2.0 |
|  | Unified | - | - | 45.9 | 194.7 | - | - | 29.1 | 26.0 | 32.1 | 12.8 |
| WLTC <br> 1st | Low | 589 | 2.98 | 18.2 | 50.9 | 5.3 | -5.3 | 26.1 | 27.8 | 19.7 | 26.3 |
|  | Middle | 433 | 5.01 | 41.6 | 72.5 | 5.4 | -7.4 | 37.0 | 24.2 | 27.2 | 11.1 |
|  | High | 455 | 7.01 | 55.5 | 97.4 | 6.5 | -7.7 | 29.0 | 28.8 | 35.2 | 7.0 |
|  | Extra-high | 323 | 8.06 | 89.8 | 125.5 | 6.4 | -4.1 | 28.5 | 27.2 | 42.1 | 2.2 |
|  | Total | 1800 | 23.06 | 46.1 | 125.5 | 6.5 | -7.7 | 29.9 | 27.1 | 29.6 | 13.4 |

The development of a World-wide harmonized Light duty Test Cycle (WLTC) which will represent typical driving conditions around the world was presented. The driving cycle was obtained from recorded in-use data ("real world" data) from different regions of the world (EU, India, Japan, Korea, USA) combined with suitable weighting factors. Over $654,000 \mathrm{~km}$ of data was collected covering a wide range of vehicle categories (M1, N1 and M2 vehicles, various engine capacities, power-to-mass ratios, manufacturers etc), over different road types (urban, rural, motorway) and driving conditions (peak, off-peak, weekend). The WLTC contains four individual sections (Low, Medium, High and Extra-high speed phase), each one composed by a sequence of idles and short trips, and has a total duration of 1800 seconds. The length of each speed phase L/M/H/ExH phases is: 589 [s], 433 [s], 455 [s] and 323 [s] respectively. The overall distance of the harmonized light duty test cycle is 23.06 km . The maximum speed is $125.5 \mathrm{~km} / \mathrm{h}$. An idle duration is $13.4 \%$ of the cycle time.

### 4.6. Modifications of the draft test cycle

The first draft needed modifying on the basis of an evaluation concerning drivability. In addition to that, EU concerned the representative of cycle dynamics. The following modifications were made during the validation phase.

### 4.6.1. WLTC version 2

In July 2011, modification of WLTC version1 was discussed over the DHC telephone conference between EU and Japan.
(1) Idling Duration

The concern which the relatively long initial idle period might impact on the effectiveness of the cycle at encouraging rapid catalyst light off was raised in the 9th DHC meeting. The determination of idling duration was reviewed and revised. Table $4-9$ shows the revised idling duration.

Table 4-9 Revised idling duration

| Phase | Cycle version | $\mathrm{T}_{\mid D 1}$ | $\mathrm{~T}_{1 D 2}$ | $\mathrm{~T}_{\mid D 3}$ | $\mathrm{~T}_{1 D 4}$ | $\mathrm{~T}_{1 D 5}$ | $\mathrm{~T}_{1 D 6}$ | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Low | Ver.1 | 1 | 3 | 8 | 18 | 28 | 86 | 144 |
|  | Ver.2 | 2 | 5 | 11 | 22 | 38 | 66 | 144 |
| Middle | Ver.1 | 7 | 41 | - | - | - | - | 48 |
|  | Ver.2 | 11 | 37 | - | - | - | - | 48 |
| High | Ver.1 | 2 | 25 | - | - | - | - | 27 |
|  | Ver.2 | 4 | 23 | - | - | - | - | 27 |
| Extra high | Ver.1 | 1 | 5 | - | - | - | - | 6 |
|  | Ver.2 | 1 | 5 | - | - | - | - | 6 |

(2) Initial idling duration

The characteristics of first ST and Idling of the day were analyzed again. The first idling of the test cycle with a duration of 11 seconds was considered to fit the median value of the first idle of the day.


The idling duration of the closest to MEDIAN is 11 s .

|  | $\mathrm{T}_{1 D 1}$ | $\mathrm{~T}_{1 D 2}$ | $\mathrm{~T}_{1 D 3}$ | $\mathrm{~T}_{1 \mathrm{D} 4}$ | $\mathrm{~T}_{1 \mathrm{D} 5}$ | $\mathrm{~T}_{1 \mathrm{D} 6}$ | Total |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Revised | 2 | 5 | 11 | 22 | 38 | 66 | 144 |

Figure 4-16 Re-analysis of Initial idling duration
(3) Initial Short trip

A separate statistical analysis has been performed in order to select the first short trip and the first idling of the driving cycle. Table 4-10 summarizes the characteristics of this analysis (the average idle duration, average short trip duration, average speed, maximum speed, distance, RPA, maximum acceleration, average acceleration, average velocity*acceleration). Based on these characteristics, from the five short trips part of the low speed phase, ST4's characteristic was the best fit with the first initial short trip of the day and therefore is the first short trip of the test cycle.

Table 4-10 Further Analysis of Initial short trip

| Item |  |  | ST duration | Average speed | Maximum speed | Distance | Maximum acceleration | Average acceleration $(+)$ | Average V*A (+) | RPA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | s | km/h | km/h | m | $\mathrm{m} / \mathrm{s}^{2}$ | $\mathrm{m} / \mathrm{s}^{2}$ | $\mathrm{m}^{2} / \mathrm{s}^{3}$ | $\mathrm{m} / \mathrm{s}^{2}$ |
| First short trip of a day | Europe | AVE | 216 | 29.6 | 49.3 | 3270 | 1.42 | 0.56 | 3.89 | 0.207 |
|  |  | S.D. | 424 | 18.3 | 28.1 | 9979 | 0.48 | 0.19 | 2.23 | 0.088 |
|  | USA | AVE | 207 | 30.5 | 55.6 | 3437 | 1.70 | 0.59 | 4.77 | 0.247 |
|  |  | S.D. | 403 | 20.4 | 29.6 | 11166 | 0.74 | 0.20 | 2.87 | 0.108 |
|  | Average | AVE | 212 | 30.0 | 52.4 | 3353 | 1.56 | 0.58 | 4.33 | 0.227 |
| WLTC | Candidate short trip of Low phase | ST1 | 19 | 4.6 | 10.8 | 25 | 0.81 | 0.48 | 0.68 | 0.189 |
|  |  | ST2 | 35 | 11.6 | 24.6 | 116 | 1.47 | 0.57 | 1.98 | 0.255 |
|  |  | ST3 | 54 | 18.0 | 33.5 | 275 | 1.25 | 0.65 | 3.19 | 0.232 |
|  |  | ST4 | 88 | 23.6 | 44.5 | 582 | 1.26 | 0.57 | 3.68 | 0.227 |
|  |  | ST5 | 249 | 28.5 | 50.9 | 1981 | 0.88 | 0.37 | 2.68 | 0.120 |

(4) Extra-High phase

Extra High phase was modified according to EU request. High acceleration portion in take off part was applied in order to represent the "ramp" acceleration. In addition to that, in order to detect OBD error, the three kinds of cruise portion of 130, 90 and $65 \mathrm{~km} / \mathrm{h}$ were applied. The WLTC version 2 was agreed to validate on drivability, traceability under the validation test phase 1.


Figure 4-17 The speed profile of the WLTC driving cycle version 2

### 4.6.2. WLTC version 2-rev

The test cycle was modified based on Validation test phase 1 test results at the 10th DHC meeting in October 2011.

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The main modifications are as follows;
(1) Acceleration portions

Acceleration portions were reviewed based on comments from the participant laboratories. Then maximum acceleration parts were set 95 percentiles of cumulative frequency in each speed range. In Extra-High phase high acceleration part ( $65-130 \mathrm{~km} / \mathrm{h}$ ) were replaced by alternative acceleration part from in-use database which matches the 95 percentiles of cumulative frequency.
(2) Deceleration portions

To avoid tire lock and/or shortage of brake power, maximum deceleration to appropriate value of $-5.31 \mathrm{~km} / \mathrm{h} / \mathrm{s}$ was set, same as maximum deceleration of UDDS.
(3) Drivability / reproducibility

Because Low speed portion (e.g. creep drive) has an adverse influence on drivability and reproducibility, minimum speed should be set to $7.5 \mathrm{~km} / \mathrm{h}$ as an average speed at the idling engine speed on the 1st gear.

The more details were described in WLTP-DHC-10-10 ${ }^{10}$.


Figure 4-18 The speed profile of the WLTC driving cycle version 2 revised

### 4.6.3. WLTC version 3

As for the test cycle of low and middle speed phase, the acceleration was enhanced, as EU indicated dynamics shortage on the world-wide harmonized base.

[^6]

Figure 4-19 The speed profile of the WLTC driving cycle version 3

### 4.6.4. WLTC version 4

In order to adjust the test cycle dynamics to the reference database, both acceleration and deceleration in low and middle speed phase were increased. In addition to that, the lowest speed during the short trip (except for start and stop) was increased to $10 \mathrm{~km} / \mathrm{h}$. As EU reconsidered extra-high speed phase, the test cycle was similar to the reference database. The 11th DHC meeting agreed to verify WLTC with validation test phase 1 b .


Figure 4-20 The speed profile of the WLTC driving cycle version 4

### 4.6.5. WLTC version 5

WLTC version5 was adopted for the validation test phase2, according to Japan' s suggestion. 15 subjects out of 31 had raised from the results of validation test phase1b from each laboratory were reviewed and revised for version5. The main improvement s are changing the lowest speed to $12 \mathrm{~km} / \mathrm{h}$ and smoothing micro transient.
The more detail was described in WLTP-DHC-12-04 ${ }^{11}$.

[^7]

Figure 4-21 The speed profile of the WLTC driving cycle version 5

### 4.6.6. WLTC version 5.1

The validation test results indicate traceability of prescribed cycle and drivability issues on compact cars produced many in emerging nations. Thus, Japan and India requested a revision to traceability of prescribed cycle in the middle and high speed phase at the 14 th DHC meeting, which was then agreed at the 15 th meeting. This cycle was decided to apply to the vehicles with $120 \mathrm{~km} / \mathrm{h}$ or lower speed as the highest velocity. Specific time table of each cycle profile is uploaded as in WLTP-DHC-16-06 ${ }^{12}$


Figure 4-22 The speed profile of the WLTC driving cycle version 5.1

### 4.6.7. WLTC version 5.3

[^8]Modification of the cycle profile was agreed as Version 5.3 at the 15 th DHC meeting, according to India's proposal. Specific time table of each cycle profile is uploaded as in WLTP-DHC-16-06 ${ }^{13}$.


Figure 4-23 The speed profile of the WLTC driving cycle version 5.3

### 4.6.8. Characteristics of WLTC

Figure 4-24 to Figure 4-29 and Table 4-11 shows The change of characteristics of WLTC.

[^9]|  | Low | Middle | High | ExHigh |
| :---: | :---: | :---: | :---: | :---: |
| Unified distribution |  |  |  |  |
| WLTC v1 |  |  |  |  |
| WLTC v2 |  |  |  |  |
| WLTC v3 |  |  |  |  |
| WLTC v4 |  |  |  |  |
| WLTC v5 |  |  |  |  |
| WLTC v5.1 |  |  |  |  |
| WLTC v5.3 |  |  |  |  |

Figure 4-24 Transition of Speed-Acceleration distribution

Table 4-11 Characteristics of WLTC

| Parameter |  | Cycle duration | Driving distance | Average speed | Max. speed | Max. acceleration | $\begin{array}{\|c\|} \text { Max. } \\ \text { Deceleration } \end{array}$ | RPA | Acceleration ratio | Deceleration ratio | Cruise ratio | Idling ratio | $\mathrm{X}^{2}$ value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | s ( h ) | km | km/h | km/h | km/h/s | km/h/s | $\mathrm{m} / \mathrm{s}^{2}$ | \% | \% | \% | \% | - |
| LOW | WWW database | - | - | 19.8 | 60.0 | - | - | 0.192 | 27.5 | 25.4 | 22.7 | 24.5 | - |
|  | WLTC v1 | 589 | 2.98 | 18.2 | 50.9 | 5.3 | -5.3 | 0.165 | 26.1 | 27.8 | 19.7 | 26.3 | 0.244 |
|  | WLTC v2 | 589 | 2.98 | 18.2 | 50.9 | 5.3 | -5.3 | 0.165 | 26.3 | 27.8 | 19.5 | 26.3 | 0.244 |
|  | WLTC v3 | 589 | 3.19 | 19.5 | 56.5 | 5.9 | -5.3 | 0.176 | 25.1 | 29.2 | 20.9 | 24.8 | 0.289 |
|  | WLTC v4 | 589 | 3.08 | 18.8 | 56.5 | 5.3 | -5.3 | 0.209 | 27.0 | 31.1 | 17.1 | 24.8 | 0.608 |
|  | WLTC v5 | 589 | 3.09 | 18.9 | 56.5 | 5.3 | -5.3 | 0.205 | 28.4 | 31.1 | 15.8 | 24.8 | 0.586 |
|  | WLTC v5.1 | 589 | 3.09 | 18.9 | 56.5 | 5.3 | -5.3 | 0.205 | 28.4 | 31.1 | 15.8 | 24.8 | 0.586 |
|  | WLTC v5.3 | 589 | 3.09 | 18.9 | 56.5 | 5.3 | -5.3 | 0.205 | 28.4 | 31.1 | 15.8 | 24.8 | 0.586 |
| MID | WWW database | - | - | 38.4 | 80.0 | - | - | 0.188 | 31.4 | 27.5 | 28.8 | 12.2 |  |
|  | WLTC v1 | 433 | 5.01 | 41.6 | 72.5 | 5.4 | -7.4 | 0.155 | 37.0 | 24.2 | 27.7 | 11.1 | 0.629 |
|  | WLTC v2 | 433 | 5.01 | 41.6 | 72.5 | 5.4 | -7.4 | 0.155 | 37.0 | 24.2 | 27.7 | 11.1 | 0.629 |
|  | WLTC v3 | 433 | 4.95 | 41.1 | 76.6 | 5.7 | -5.3 | 0.184 | 33.7 | 29.6 | 26.1 | 10.6 | 0.613 |
|  | WLTC v4 | 433 | 4.74 | 39.4 | 76.6 | 5.6 | -5.3 | 0.198 | 36.0 | 30.3 | 23.1 | 10.6 | 0.649 |
|  | WLTC v5 | 433 | 4.76 | 39.5 | 76.6 | 5.7 | -5.4 | 0.196 | 36.0 | 30.3 | 23.1 | 10.6 | 0.650 |
|  | WLTC v5.1 | 433 | 4.72 | 39.3 | 76.6 | 4.6 | -5.3 | 0.189 | 37.9 | 29.1 | 22.4 | 10.6 | 0.751 |
|  | WLTC v5.3 | 433 | 4.76 | 39.5 | 76.6 | 5.7 | -5.4 | 0.196 | 36.0 | 30.3 | 23.1 | 10.6 | 0.650 |
| HIGH | WWW database | - | - | 58.0 | 110.0 | - | - | 0.156 | 31.3 | 27.2 | 35.5 | 6.0 |  |
|  | WLTC v1 | 455 | 7.01 | 55.5 | 97.4 | 6.5 | -7.7 | 0.144 | 29.0 | 28.8 | 35.2 | 7.0 | 0.962 |
|  | WLTC v2 | 455 | 7.01 | 55.5 | 97.4 | 6.5 | -7.7 | 0.144 | 29.0 | 28.8 | 35.2 | 7.0 | 0.962 |
|  | WLTC v3 | 455 | 7.05 | 55.8 | 97.4 | 6.5 | -5.3 | 0.143 | 28.8 | 28.8 | 36.0 | 6.4 | 0.869 |
|  | WLTC v4 | 455 | 7.06 | 55.9 | 97.4 | 6.5 | -5.3 | 0.137 | 27.0 | 27.3 | 39.3 | 6.4 | 1.065 |
|  | WLTC v5 | 455 | 7.16 | 56.6 | 97.4 | 5.7 | -5.4 | 0.135 | 26.8 | 27.9 | 38.9 | 6.4 | 1.113 |
|  | WLTC v5.1 | 455 | 7.12 | 56.4 | 97.4 | 5.7 | -5.4 | 0.122 | 28.1 | 27.0 | 38.5 | 6.4 | 1.137 |
|  | WLTC v5.3 | 455 | 7.16 | 56.7 | 97.4 | 5.7 | -5.4 | 0.132 | 29.0 | 27.7 | 36.9 | 6.4 | 1.008 |
| Ex-HIGH | WWW database | - | - | 86.8 | 194.7 | - | - | 0.108 | 25.7 | 23.4 | 48.9 | 2.0 |  |
|  | WLTC v1 | 323 | 8.06 | 89.8 | 125.5 | 6.4 | -4.1 | 0.108 | 28.5 | 27.2 | 42.1 | 2.2 | 1.026 |
|  | WLTC v2 | 323 | 7.72 | 86.0 | 132.0 | 7.4 | -6.8 | 0.127 | 25.4 | 25.4 | 47.7 | 1.5 | 5.312 |
|  | WLTC v3 | 323 | 7.67 | 85.4 | 130.4 | 6.1 | -5.3 | 0.126 | 26.9 | 25.7 | 45.8 | 1.5 | 4.413 |
|  | WLTC v4 | 323 | 8.25 | 92.0 | 131.3 | 3.7 | -4.4 | 0.125 | 36.2 | 31.6 | 30.7 | 1.5 | 2.779 |
|  | WLTC v5 | 323 | 8.25 | 92.0 | 131.3 | 3.7 | -4.4 | 0.125 | 37.2 | 32.2 | 29.1 | 1.5 | 2.678 |
|  | WLTC v5.1 | 323 | 8.25 | 92.0 | 131.3 | 3.7 | -4.4 | 0.125 | 37.2 | 32.2 | 29.1 | 1.5 | 2.678 |
|  | WLTC v5.3 | 323 | 8.25 | 92.0 | 131.3 | 3.7 | -4.4 | 0.125 | 37.2 | 32.2 | 29.1 | 1.5 | 2.678 |
| $\underset{(\mathrm{L}-\mathrm{ExH})}{\mathrm{ALL}}$ | WWW database | - | - | 45.9 | 194.7 | - | - | 0.167 | 29.1 | 26.0 | 32.1 | 12.8 |  |
|  | WLTC v1 | 1800 | 23.06 | 46.1 | 125.5 | 6.5 | -7.7 | 0.137 | 29.9 | 27.1 | 29.6 | 13.4 | 0.204 |
|  | WLTC v2 | 1800 | 22.72 | 45.4 | 132.0 | 7.4 | -7.7 | 0.144 | 29.4 | 26.8 | 30.5 | 13.3 | 0.738 |
|  | WLTC v3 | 1800 | 22.86 | 45.7 | 130.4 | 6.5 | -5.3 | 0.151 | 28.4 | 28.6 | 30.4 | 12.6 | 0.652 |
|  | WLTC v4 | 1800 | 23.14 | 46.3 | 131.3 | 6.5 | -5.3 | 0.155 | 30.8 | 30.0 | 26.6 | 12.6 | 0.657 |
|  | WLTC v5 | 1800 | 23.26 | 46.5 | 131.3 | 5.7 | -5.4 | 0.153 | 31.4 | 30.3 | 25.8 | 12.6 | 0.641 |
|  | WLTC v5.1 | 1800 | 23.19 | 46.4 | 131.3 | 5.7 | -5.4 | 0.148 | 32.2 | 29.8 | 25.5 | 12.6 | 0.681 |
|  | WLTC v5.3 | 1800 | 23.27 | 46.5 | 131.3 | 5.7 | -5.4 | 0.152 | 31.9 | 30.2 | 25.3 | 12.6 | 0.609 |



Figure 4-25 Cumulative frequency of multiplication of speed and acceleration ( $\mathrm{v}^{*}$ a) in Low phase


Figure 4-26 Cumulative frequency of multiplication of speed and acceleration ( $\mathrm{v}^{*}$ a) in Middle phase


Figure 4-27 Cumulative frequency of multiplication of speed and acceleration ( $v^{*}$ a) in High phase


Figure 4-28 Cumulative frequency of multiplication of speed and acceleration ( $v^{*}$ a) in Extra high phase


Figure 4-29 Cumulative frequency of multiplication of speed and acceleration (v*a) in WLTC

### 4.7. WLTC for Low Powered vehicle

India expressed substantial concerns with respect to the drivability of the test cycle for their low powered vehicles. These vehicles would have to drive a special cycle consisting of a modified low, medium and high speed part in the 10th DHC meeting. The cycle development for low powered vehicles was agreed at the 11th DHC meeting with the discussion on the definition of "low powered vehicles".
India submitted additional in-use driving data specialized in low powered vehicles. The cycle for the low powered vehicles were drawn up based on driving data of the vehicles with power to mass ratio $35 \mathrm{tW} / \mathrm{t}$ or lower from the additional and existing data. Traceability of prescribed cycle and drivability were evaluated with validation 1 b and 2. Then the revised version 2.0 was agreed.

The speed profiles of the WLTC for low powered vehicle are shown in Figure 4-30 and Figure 4-31 ${ }^{14}$.

[^10]Informal document GRPE-67-03
( $67^{\text {th }}$ GRPE, 14 November 2013, agenda item 2)


Figure 4-30 The speed profile of the WLTC Class 1 version 2.0


Figure 4-31 The speed profile of the WLTC Class 2 version 2.0
4.8. Vehicle classification and applicable test cycle

The vehicle classification is one of the important issues of the WLTP development process. From practical reasons, the cycle allocation was agreed during 15th DHC meeting on December 2012 as shown in Figure31b. (WLTP-DHC-15-04)


Figure 4 31b Vehicle classifications of WLTC

### 4.9. Down scale procedure

### 4.9.1. Preliminary note

The WLTP vehicle classification is based on the ratio between rated power and kerb mass (pmr). Based on an analysis of the dynamics of the in-use data the following classification was agreed:

1. Class 1: $\mathrm{pmr}<=22 \mathrm{~W} / \mathrm{kg}$,
2. Class 2: $22 \mathrm{~W} / \mathrm{kg}<\mathrm{pmr}<=34 \mathrm{~W} / \mathrm{kg}$,
3. Class 3: pmr $>34 \mathrm{~W} / \mathrm{kg}$.

Consequently, 3 different WLTC versions were developed according to the dynamic potentials of the different classes. The maximum speeds of the different cycle versions and phases are shown in Table 4-12.

Table 4-12 Maximum speeds of the cycle phases

| Vehicle class | Cycle version | v_max for cycle phase in km/h |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | low | medium | high | extra high |
| 1 | 2 | 49.1 | 64.4 |  |  |
| 2 | 2 | 51.4 | 74.7 | 85.2 | 123.1 |
| 3 | $5.1 / 5.3$ | 56.5 | 76.6 | 97.4 | 131.3 |

During the validation 2 phase some vehicles with pmr values close to the borderlines had problems to follow the cycle speed trace within the tolerances $(+/-2 \mathrm{~km} / \mathrm{h},+/-1 \mathrm{~s})$. The following figures show one example per vehicle class.


Figure 4-32 Speed trace of a class 1 vehicle with drivability problems


Figure 4-33 Speed trace of a class 2 vehicle with drivability problems


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Figure 4-34 Speed trace of a class 3 vehicle with drivability problems

The question to be answered was, how to proceed with such vehicles. Three possibilities were discussed:

1. Follow the trace as good as possible,
2. Apply a cap on the maximum speed of the vehicle,
3. Downscale the cycle for those sections where the driveability problems occur.

The first possibility can lead to excessively high percentages of full load (wot) operation and would create a burden for those vehicles compared to vehicles without driveability problems. The second possibility was found to be not very effective. It works for some vehicle configurations but does not work for others. The third possibility was found to be more effective and the technical justification is given in the following paragraphs.

The calculation equations and calculation coefficients are based on correlation analyses and were modified in a second step in order to optimise the efficiency of the method.

The calculation of the downscaling factor is based on the ratio between the maximum required power of the cycle phases where the downscaling has to be applied and the rated power of the vehicle. The maximum required power within the cycle occurs at that time with the combination of high vehicle speed and high acceleration values. That means that the road load coefficients as well as the test mass are considered.

### 4.9.2. Cycle downscaling, class 1 vehicles

Since the driveability problems are exclusively related to the medium speed phase of the class 1 cycle, the downscaling is related to those sections of the medium speed phase, where the driveability problems occur (see Figure 4-35).


Figure 4-35 Downscaled medium speed phase of the class 1 WLTC

For the class 1 cycle the downscaling period is the time period between second 651 and second 906 . Within this time period the acceleration for the original cycle is calculated using the following equation:

$$
\text { a_orig_i }=\left(\mathbf{v} \_\mathbf{i}+1-\mathbf{v}_{-} \mathbf{i}\right) / \mathbf{3 . 6}
$$

## Equation 1

$\mathrm{v} \_\mathrm{i}$ is the vehicle speed in $\mathrm{km} / \mathrm{h}$, i is the time between 651 and 906 s .
The downscaling is first applied in the time period between second 651 and 848 . Second 848 is the time where the maximum speed of the extra high speed phase is reached. The downscaled speed trace is then calculated using the following equation:

```
v_dsc_i+1 = v_dsc_i + a_orig_i * (1 - dsc_factor) * 3.6
```


## Equation 2

with $\mathrm{i}=651$ to $848 . \mathrm{v}_{-}$dsc_i $=$v_orig_i for $\mathrm{i}=651$.
In order to meet the original vehicle speed at second 907 a correction factor for the deceleration is calculated using the following equation:

$$
\text { f_corr_dec }=\left(\mathbf{v} \_d s c \_848-36,7\right) /(\text { v_orig_848-36,7) }
$$

## Equation 3

$36,7 \mathrm{~km} / \mathrm{h}$ is the original vehicle speed at second 907.
The downscaled vehicle speed between 849 and 906 s is then calculated using the following equation:

$$
\text { v_dsc_i = v_dsc_i-1 + a_orig_i-1 * f_corr_dec * } 3.6
$$

## Equation 4

with $\mathrm{i}=849$ to 906 .

### 4.9.3. Downscaling procedure for class 2 vehicles

Since the driveability problems are exclusively related to the extra high speed phases of the class 2 and class 3
cycles, the downscaling is related to those sections of the extra high speed phases, where the driveability problems occur (see Figure 4-36).


Figure 4-36 Downscaled extra high speed phase of the class 2 WLTC

For the class 2 cycle the downscaling period is the time period between second 1520 and second 1742 . Within this time period the acceleration for the original cycle is calculated using the following equation:

$$
\text { a_orig_i }=\left(v_{-} \mathbf{i}+1-v_{-} \mathbf{i}\right) / \mathbf{3 . 6}
$$

## Equation 5

$\mathrm{v} \_i$ is the vehicle speed in $\mathrm{km} / \mathrm{h}$, i is the time between 1520 and 1742 s .
The downscaling is first applied in the time period between second 1520 and 1724. Second 1724 is the time where the maximum speed of the extra high speed phase is reached. The downscaled speed trace is then calculated using the following equation:

$$
\mathbf{v}_{-} \mathbf{d s c} \_\mathbf{i}+1=\mathbf{v}^{\prime} \mathbf{d s c} \_\mathbf{i}+\mathbf{a} \_ \text {orig_i} *\left(1-d s c \_f a c t o r\right) * 3.6
$$

## Equation 6

with $\mathrm{i}=1520$ to 1724 . v _dsc_ $\mathrm{i}=\mathrm{v}_{\text {_orig_i }}$ for $\mathrm{i}=1520$.
In order to meet the original vehicle speed at second 1743 a correction factor for the deceleration is calculated using the following equation:

$$
\text { f_corr_dec }=\left(\mathbf{v} \_d s c \_1725-90,4\right) /\left(v_{1}\right. \text { orig_1725-90,4) }
$$

## Equation 7

$90,4 \mathrm{~km} / \mathrm{h}$ is the original vehicle speed at second 1743.
The downscaled vehicle speed between 1726 and 1742 s is then calculated using the following equation:

$$
\mathbf{v} \_d s c_{-} \mathbf{i}=\mathbf{v}^{\prime} \mathbf{d s c} \_\mathbf{i}-1+\mathbf{a}_{-} \text {orig_i-1 } * \mathbf{f}_{-} \text {corr_dec } * 3.6
$$

## Equation 8

with $\mathrm{i}=1726$ to 1742 .

### 4.9.4. Downscaling procedure for class 3 vehicles

Figure 4-37 shows an example for a downscaled extra high speed phase of the class 3 WLTC.


Figure 4-37 Downscaled extra high speed phase of the class 3 WLTC

For the class 3 cycle this is the period between second 1533 and second 1763 . Within this time period the acceleration for the original cycle is calculated using the following equation:

$$
\text { a_orig_i }=\left(v_{-} \mathbf{i}+1-v_{-} i\right) / 3.6
$$

## Equation 9

$v_{-} i$ is the vehicle speed in $\mathrm{km} / \mathrm{h}, \mathrm{i}$ is the time between 1533 and 1762 s .
The downscaling is first applied in the time period between second 1533 and 1724. Second 1724 is the time where the maximum speed of the extra high speed phase is reached. The downscaled speed trace is then calculated using the following equation:

$$
\mathbf{v} \_d s c \_i+1=v_{-} d s c \_i+\mathbf{a}_{-} \text {orig_i } *(1-\text { dsc_factor }) * 3.6
$$

## Equation 10

with $\mathrm{i}=1533$ to 1723 . $\mathrm{v}_{-}$dsc_ $\mathrm{i}=\mathrm{v}_{\text {_ }}$ orig_i for $\mathrm{i}=1533$.
In order to meet the original vehicle speed at second 1763 a correction factor for the deceleration is calculated using the following equation:
f_corr_dec = (v_dsc_1724-82.6) / (v_orig_1724-82.6)

## Equation 11

$82.6 \mathrm{~km} / \mathrm{h}$ is the original vehicle speed at second 1763.
The downscaled vehicle speed between 1725 and 1762 s is then calculated using the following equation:

$$
\mathbf{v}_{-} \mathbf{d s c}_{-} \mathbf{i}=\text { v_dsc_i-1 + a_orig_i-1 } * \mathbf{f}_{-} \text {corr_dec } * 3.6
$$

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with $\mathrm{i}=1725$ to 1762.

### 4.9.5. Results of model calculations

The development of the proposal for downscaling factors is based on calculations performed with a modified version of the WLTP gearshift calculation tool, which provides also estimates of the CO 2 emissions.

The following calculations were performed:

- Class 3 vehicles: 133 configurations with vmax between $90 \mathrm{~km} / \mathrm{h}$ and $146 \mathrm{~km} / \mathrm{h}, 96$ of them needed downscaling, 37 did not.
- Class 2 vehicles: 164 configurations with vmax between $90 \mathrm{~km} / \mathrm{h}$ and $141 \mathrm{~km} / \mathrm{h}, 124$ of them needed downscaling, 40 did not.
- Class 1 vehicles: 78 configurations with vmax between $58 \mathrm{~km} / \mathrm{h}$ and $129 \mathrm{~km} / \mathrm{h}, 23$ of them needed downscaling, 55 did not .

The maximum speeds were calculated from the transmission data and the driving resistance coefficients used for the different vehicle configurations. For one part of the configurations the default values of the driving resistance coefficients, provided by the model, were used. Since these coefficients are based on existing European legislation and thus do not reflect the modifications currently discussed within the GTR development process, calculations were performed for additional configurations with varied driving resistance coefficients. These driving resistance coefficients were chosen from a data pool provided by vehicle manufacturers, TUG and TNO.

For the calculations min, ave and max values for $\mathrm{f} 0, \mathrm{f} 1$ and f 2 were used for the following vehicle categories:

- Subcompact cars,
- Compact cars,
- Medium cars,
- Large cars,
- Small N1,
- Medium N1,
- Large N1.

According to the aim of the analysis the focus was set on subcompact, compact cars and N1 vehicles.

The necessary downscaling factors were determined by a stepwise increase of the downscaling factor fdsc by $1 \%$, starting at $1 \%$ for vehicles with speed trace tolerance violations until no violations occurred.

The ratio between the maximum power demand (including acceleration power) within the extra high speed phase (medium speed phase for class 1 vehicles) and the rated power correlates reasonably with the necessary downscaling factors. This ratio is called rmax.

The cycle time i where the maximum power (including acceleration power) is required is

$$
\begin{aligned}
& \circ \quad 764 \mathrm{~s} \text { for class } 1, \mathrm{v}=61.4 \mathrm{~km} / \mathrm{h}, \mathrm{a}=0.22 \mathrm{~m} / \mathrm{s}^{2}, \\
& \circ \\
& \circ \\
& \hline
\end{aligned}
$$

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```
- 1566 s for class \(3, \mathrm{v}=111.9 \mathrm{~km} / \mathrm{h}, \mathrm{a}=0.5 \mathrm{~m} / \mathrm{s}^{2}\).
```

The power demand can easily be calculated from the driving resistance coefficients, the mass of the vehicle and the cycle parameter vehicle speed and acceleration.

Preq, $\max =(\mathrm{f} 0 * \mathrm{v}+\mathrm{f} 1 * \mathrm{v} 2+\mathrm{f} 2 * \mathrm{v} 3) / 3600+\mathrm{kr} *$ mtest $^{*} \mathrm{a}^{*} * \mathrm{v} / 3600$
with v - vehicle speed in $\mathrm{km} / \mathrm{h}$, a-acceleration in $\mathrm{m} / \mathrm{s}^{2}$,
mtest - test mass in kg and P in kW .
kr represents the rotational inertia and was set to 1,1 .
The driving resistance coefficients f0, f1 and f2 have to be determined by coast down measurements or an equivalent method. The available power depends on the full load power curve (wot curve) and the transmission design. Average wot curves for Petrol and Diesel vehicles as provided by Stefan Hausberger were used for the calculations.

The transmission designs were taken from manual transmission vehicles either from the WLTP in-use database or the validation 2 database. In some cases the transmission design was modified in order to assess the influence on driveability. For the available power a safety margin of $10 \%$ was applied to the wot curves.

In order to illustrate the power demand and the available power both values were calculated for each second of the WLTC and plotted against the vehicle speed. The driveability was checked by a comparison of the actual speed, the set speed (original or downscaled) and the tolerance band.

### 4.9.6. Results for class 3 vehicles

Figure 4-38 shows the necessary downscaling factors versus the ratios between the maximum required power and rated power for class 3 vehicles. Since the maximum power demand is related to $v=111.9 \mathrm{~km} / \mathrm{h}$, vehicles with vmax above and below this threshold are separated. For vehicles with vmax below $112 \mathrm{~km} / \mathrm{h} \mathrm{r} \_$max is only a theoretical parameter.

In addition to that vehicles with 4 speed transmissions and transmissions with more than 4 gears are separated.
Before the results are discussed it should be clarified if the maximum power demand at a specific second is a suitable parameter. Figure 4-39 shows a comparison of this parameter with average values over several seconds. The correlation is so strong, that the maximum values can be used.

But Figure 4-38 shows significant differences between the already mentioned subgroups. Vehicles with 4 speed transmissions require on average higher downscaling factors (fdsc) than vehicles with transmissions with more than 4 gears and vehicles with vmax values below the threshold require downscaling only at high rmax values (above 130\%).

On the other hand, the variation range of fdsc at given rmax values is significantly higher for vehicles with 4speed transmissions compared to vehicles with transmissions with more than 4 gears. Some of the vehicles with 4speed transmissions fit well to the group with transmissions with more than 4 gears.

The most extreme examples are two vehicles with $\operatorname{rmax}=134 \%$. One requires a fdsc of $35 \%$, the other only $21 \%$.


Figure 4-38 Necessary downscaling factor versus $r_{-}$max for class $\mathbf{3}$ vehicles


Figure 4-39 Comparison of Ptot_max and Ptot_ave

The differences between both vehicles are only related to the transmission design. Rated power and test mass are exactly the same. The speed traces of both vehicles for the extra high speed phase are shown in Figure 4-40 and Figure 4-41. The corresponding power values are shown in Figure 4-42 and Figure 4-43.
Vehicle 361 has higher driveability problems than vehicle 362 , although vmax of vehicle 361 is slightly higher than for vehicle 362. The reason is the disadvantageous transmission design of vehicle 361 compared to vehicle 362. For vehicle 361 the highest power demand corresponds to a valley of the available power between gear 3 and gear 4 (see Figure 4-42), while for vehicle 362 the highest demand coincides with the highest available power in 4. Gear (see Figure 4-43).


Figure 4-40 Speed trace of the extra high speed phase for vehicle 361


Figure 4-41 Speed trace of the extra high speed phase for vehicle 362


Figure 4-42 Corresponding power values for vehicle 361


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Figure 4-43 Corresponding power values for vehicle 362

Since vehicle 361 has a higher full load (wot) percentage and a higher fuel consumption ( $2 \%$ in total and almost $5 \%$ in the extra high speed phase) than vehicle 362.

Similar results were found for other 4speed examples and there are also a few examples of disadvantageous transmission design for vehicles with more than 4 gears. Such disadvantageous examples should not determine the forecast function for fdsc and the transmission design should not be included into the calculation, so that vehicles with automatic transmission can still be included. The results for vehicles with more than 4 gears and vmax $>112$ $\mathrm{km} / \mathrm{h}$ can be approximated by a 2 nd degree polynomial regression curve (see Figure 4-38).

For simplification reasons this function was approximated by a linear curve starting at $\mathrm{rmax}=100 \%$ with $\mathrm{fdsc}=$ $0 \%$ and reaching fdsc $=32.5 \%$ at $\operatorname{rmax}=150 \%$. For vehicles with $\mathrm{vmax}<=112 \mathrm{~km} / \mathrm{h}$, the approximation function for fdsc is the same as above, but the downscaling is only applied for vehicles with rmax $>130 \%$.

### 4.9.7. Results for class 2 vehicles

Figure 4-44 shows similar results as Figure $4-38$, but for class 2 vehicles. The reference speed for the determination of the max. power demand is $110 \mathrm{~km} / \mathrm{h}$, but the analysis of the calculation results showed that 105 $\mathrm{km} / \mathrm{h}$ is a better separator between the subgroups. Below this threshold no downscaling needs to be applied. Above this threshold a similar correlation of the fdsc values with the rmax values was found but with a less steep slope than for class 3 vehicles. And the differences between vehicles with 4 gears and more than 4 gears are less pronounced.


Figure 4-44 Necessary downscaling factor versus $r_{\text {_ }}$ max for class $\mathbf{2}$ vehicles

The linear approximation curve starts also at $\mathrm{rmax}=100 \%$ and $\mathrm{fdsc}=0 \%$ and goes to $\mathrm{fdsc}=30 \%$ at $\mathrm{rmax}=150 \%$. The differences in fdsc for a given rmax between different vehicles (up to $10 \%$ for fdsc for both subgroups) are also caused by differences in the transmission design.

### 4.9.8. Results for class 1 vehicles

The results for class 1 vehicles are shown in Figure 4-45. The reference speed for the maximum power demand is $61.4 \mathrm{~km} / \mathrm{h}$. Therefore $61 \mathrm{~km} / \mathrm{h}$ was chosen as threshold. First of all must be mentioned that all vehicles with more than 4 gears had vmax values above the threshold and rmax values between $43 \%$ and $105 \%$. None of them needed downscaling.

Furthermore, the results for vehicles with 4 speed transmissions above and below the threshold do not show significant differences. Therefore it is proposed to use the linear approximation curve as shown in Figure 4-45 for all class 1 vehicles. This curve starts at $\mathrm{rmax}=100 \%$ with fdsc $=0 \%$ and goes up to fdsc $=26 \%$ at $\mathrm{rmax}=150 \%$.


Figure 4-45 Necessary downscaling factor versus $r_{-}$max for class 1 vehicles

### 4.9.9. Comparison between necessary downscaling factors and factors obtained from the linear regression curves

In order to check the results obtained by the linear approximation curves, calculations with the downscaling factors forecasted by these curves were performed in a second step.

Figure 4-46 shows the forecasted f_dsc values versus the necessary values for class 3 vehicles. The percentage of vehicles with speed trace violations drops from $72 \%$ to $27 \%$, the total number of violations drops down to $17.5 \%$. The wot percentage for the extra high speed phase is significantly reduced (by up to $30 \%$ ) compared to the situation without downscaling. The reduction in fuel consumption compared to the situation without downscaling is $1.6 \%$ on average and $4.2 \%$ at maximum.

Figure 4-47 shows the forecasted f_dsc values versus the necessary values for class 2 vehicles. The percentage of vehicles with speed trace violations drops from $75 \%$ to $27 \%$, the total number of violations drops down to $13 \%$. The wot percentage for the extra high speed phase is significantly reduced (by up to $40 \%$ ) compared to the situation without downscaling. The reduction in fuel consumption compared to the situation without downscaling is $1.3 \%$ on average and $5.5 \%$ at maximum.

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Figure $4-48$ shows the forecasted f_dsc values versus the necessary values for class 1 vehicles. The percentage of vehicles with speed trace violations drops from $30 \%$ to $13 \%$, the total number of violations drops down to $4 \%$. The wot percentage for the medium speed phase is significantly reduced (by up to $13 \%$ ) compared to the situation without downscaling. The maximum value with downscaling is $20.5 \%$ for the medium speed part. The reduction in fuel consumption compared to the situation without downscaling is $1 \%$ on average and $2.9 \%$ at maximum.


Figure 4-46: Comparison between necessary downscaling factors and factors obtained from the linear regression curves, class 3


Figure 4-47: Comparison between necessary downscaling factors and factors obtained from the linear regression curves, class 2


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Figure 4-48: Comparison between necessary downscaling factors and factors obtained from the linear regression curves, class 1

### 4.9.10. Determination of the downscaling factor

The downscaling factor fdsc is a function of the ratio between the maximum required power of the cycle phases where the downscaling has to be applied and the rated power of the vehicle (Prated).

This ratio is named rmax, the maximum required power is named Preq, max. It is related to a specific time i in the cycle trace.

Preq, max, i in kW is calculated from the driving resistance coefficients f 0 , f 1 , f 2 and the test mass mtest as follows:

Preq, max, $\mathrm{i}=\left(\mathrm{f} 0 * \mathrm{vi}+\mathrm{f} 1^{*}\right.$ vi $2+\mathrm{f} 2 *$ vi $3+1.1 *$ mtest $*$ vi ${ }^{*}$ ai $) / 3600$ Equation 13
with f0 in $\mathrm{N}, \mathrm{f} 1$ in $\mathrm{N} /(\mathrm{km} / \mathrm{h})$ and f 2 in $\mathrm{N} /(\mathrm{km} / \mathrm{h}) 2$, mtest in kg
The cycle time i where the maximum power is required is

- 764 s for class 1 ,
- 1574 s for class 2 and
- 1566 s for class 3

The corresponding vehicle speed values vi and acceleration values ai are as follows:

- $\quad \mathrm{vi}=\quad 61.4 \mathrm{~km} / \mathrm{h}, \mathrm{ai}=0.22 \mathrm{~m} / \mathrm{s}^{2}$ for class 1 ,
- $\quad \mathrm{vi}=109.9 \mathrm{~km} / \mathrm{h}, \mathrm{ai}=0.36 \mathrm{~m} / \mathrm{s}^{2}$ for class 2 ,
- $\quad \mathrm{vi}=111.9 \mathrm{~km} / \mathrm{h}, \mathrm{ai}=0.50 \mathrm{~m} / \mathrm{s}^{2}$ for class 3,

The driving resistance coefficients f0, f1 and f2 have to be determined by coast down measurements or an equivalent method.
rmax is calculated using the following equation:

```
rmax = Preq, max, i / Prated Equation 14
```

The downscaling factor fdsc is calculated using the following equation:

```
fdsc = 0, if rmax < r0
a* rmax +b, if rmax >= r0 Equation 15
```

The calculation parameter/coefficients r0, a1 and b1 are as follows:.

- Class 1: $\mathrm{r} 0=100 \%, \mathrm{a}=0.54, \mathrm{~b}=-0.54$
- Class 2:
- $\quad \max >105 \mathrm{~km} / \mathrm{h}: \mathrm{r} 0=100 \%, \mathrm{a}=0.41, \mathrm{~b}=-0.41$,
- $\operatorname{vmax}<=105 \mathrm{~km} / \mathrm{h}$ : no downscaling,
- Class 3:
- $\operatorname{vmax}>112 \mathrm{~km} / \mathrm{h}: \mathrm{r} 0=100 \%, \mathrm{a}=0.65, \mathrm{~b}=-0.65$,
- $\operatorname{vmax}<=112 \mathrm{~km} / \mathrm{h}: \mathrm{r} 0=130 \%, \mathrm{a}=0.65, \mathrm{~b}=-0.65$.

The vmax thresholds are related to the reference speeds for the determination of the maximum required power. [Open point: should there be a lower limit for fdsc (e.g. 3\%). In other words, shall fdsc < threshold be

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## disregarded?]

### 4.9.11. Additional requirements

If a vehicle is tested under different configurations in terms of test mass and driving resistance coefficients, the worst case (highest Preq, max, i value) has to be used for the determination of the downscaling factor and the resulting downscaled cycle shall be used for all measurements.

If the maximum speed of the vehicle is lower than the maximum speed of the downscaled cycle, the vehicle shall be driven with its maximum speed in those cycle periods where the cycle speed is higher than the maximum speed of the vehicle.

If the unlikely situation occurs that the vehicle cannot follow the speed trace of the downscaled cycle within the tolerance for specific periods, it shall be driven with the accelerator pedal fully engaged during these periods.

## 5. Gearshift procedure development

### 5.1. Analysis of gear use in the WLTP in-use database, discussion of alternative approaches

The development of the gearshift prescriptions for vehicles with manual transmissions was based on an analysis of the gear use in the WLTP in-use database. This database contains 128 M1 and 29 N 1 vehicles with manual transmissions and engine speed signals that allowed a sufficiently good gear determination. 3 vehicles have 4 speed gearboxes, 115 vehicles have 5 speed gearboxes and 39 vehicles have 6 speed gearboxes.

The approach for gearshift detection was as follows:
In a first step the ratio between engine speed in min-1 and vehicle speed in $\mathrm{km} / \mathrm{h}$ was calculated and added to the databases. The appropriate ratios for the different gears were then derived from the frequency distributions of the ratios. The gears were then assigned to the data by applying a window of $+/-10 \%$ to these ratios. Figure 5-1 shows a Diesel vehicle with a 6speed gearbox as an example.


Figure 5-1: Example of engine speed versus vehicle speed plot for a 6speed Diesel vehicle from the WLTP in-use database

Based on this up- and downshifts were detected and collected in an additional database table for consecutive time periods, allowing 1 s for clutch operation in between. The analysis of the gear use was performed separately but with intensive information exchange by JARI, Eva Ericsson and Heinz Steven. The most important result was, that the gearshift behaviour is much more influenced by individual driving behaviour rather than by technical

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parameter of the vehicles or the transmissions. Since type approval is more related to the technical parameters of the vehicle rather than to individual driving behaviour and since the technical designs of the transmissions have changed significantly over the last decades and will keep changing also in future, there was no need to stick too much to the in-use database results, which reflects the situation 5 to 10 years ago.

As results of the data analysis and assessment the following two alternative approaches were proposed and discussed:

- Vehicle speed based gearshifts,
- Normalised engine speed based gearshifts

The vehicle speed based gearshift approach defines shiftpoints as function of vehicle speed and acceleration. For a given cycle this results in fixed vehicle speeds. But this approach requires a separation of M1 and N1 vehicles. The engine speed based gearshift approach determines normalised engine upshift speeds as function of the power to mass ratio of the vehicle. The shift speeds are the same for each gear and independent of the number of gears.

The Advantage of the vehicle speed based prescriptions is the simplicity and easy implementation into drivers aids of test benches and that no vehicle specific input data is needed. The disadvantages are that different gearbox designs in terms of numbers of gears cause differences in average engine speeds against the trend in real traffic and that driveability problems could occur for low powered vehicles, especially for N1 vehicles.

The advantage of the engine speed based approach is the independency from the gearbox design, the disadvantage is the need of vehicle specific input data like power to mass ratio, rated speed, idling speed and transmission ratios Driveability problems could also occur depending on the transmission design.

The validation 1 tests showed driveability problems for both approaches, which could only be solved or reduced by more specific requirements. In case of the vehicle speed based approach a further separation into vehicle subgroups would have been needed. In case of the engine speed based approach the consideration of the engine power demand and the available power would have been required.

Since the latter was seen to be more appropriate and effective with respect to future transmission developments, the vehicle speed based proposal was skipped and the engine speed based proposal was further improved.

With respect to future developments one of the vehicle manufacturers developed gearshift prescriptions that are purely based on the individual acceleration performance of a vehicle under test. This means that in addition to rated engine speed and power and idling speed also the test mass, the full load power curve, the driving resistance coefficients $f_{0}, f_{1}$ and $f_{2}$ and the gear ratios were needed as input data. This proposal was merged with the engine speed based approach used for validation 1 and built the basis for the further development.

In order to reflect practical use as well as fuel efficient driving behaviour as much as possible, the prescriptions are based on the balance between the power required for driving resistance and acceleration and the power provided by the engine in all possible gears at a specific cycle phase.

The developed gearshift prescriptions were used for the validation 2 tests and further amended based on the comments/recommendations from the validation 2 participants. This led to the following prescriptions.

### 5.2. Input data

The required input data is described below and summarized in Table 5-1.
The following data is required to calculate the gears to be used when driving the cycle on a test bench:
(a) $\mathrm{P}_{\text {rated }}$, rated engine power. The maximum power of the engine as declared by the manufacturer.
(b) s, rated engine speed. The engine speed at which an engine develops its maximum power. If the maximum power is developed over an engine speed range, $s$ is determined by the mean of this range.
(c) $\mathrm{n}_{\text {idle }}$, idling speed as defined in Annex 1 of ECE R 83
(d) $\mathrm{n}_{\text {min_drive }}$, minimum engine speed for short trips, and is used to define downshifts. The minimum value is determined by the following equation:

$$
\begin{equation*}
\mathrm{n}_{\text {min_drive }}=\mathrm{n}_{\text {idle }}+(0.125) \times\left(\mathrm{s}-\mathrm{n}_{\text {idle }}\right) \tag{1}
\end{equation*}
$$

Higher values can be used if requested by the manufacturer.
(e) $\mathrm{i}=1$ to $\mathrm{ng}_{\text {max }}$ determine the gear number
(f) $\mathrm{ng}_{\text {max }}$, the number of gears
(g) $n d v_{\mathrm{i}}$, a ratios determined by dividing n in $\min ^{-1}$ by v in $\mathrm{km} / \mathrm{h}$ for each gear $\mathrm{i}, \mathrm{i}=1$ to $\mathrm{ng}_{\text {max }}$.
(h) $\mathrm{m}_{\mathrm{t}}$, test mass of the vehicle in kg .
(i) $f_{0}, f_{1}, f_{2}$, driving resistance coefficients as defined in Annex 4.
(j) full load power curve, normalized to rated power and (rated speed - idling speed).

Table 5-1 Necessary input data for the gear use calculation

| parameter | unit | definition/description |
| :---: | :---: | :---: |
| $\mathbf{P}_{\text {rated }}$ | kW | The maximum power of the engine as declared by the manufacturer. |
| s | $\min ^{-1}$ | Rated engine speed, the engine speed at which an engine develops its maximum power. If the maximum power is developed over an engine speed range, $s$ is determined by the mean of this range. |
| $\mathbf{n}_{\text {idle }}$ | $\min ^{-1}$ | Idling speed, the engine speed when the gear lever is in neutral and the vehicle is not in motion. |
| $\mathbf{n}_{\text {min_drive }}$ | $\min ^{-1}$ | minimum engine speed for gear numbers $\geq 3$ when the vehicle is in motion. The minimum value is determined by $n_{\text {idlle }}+0,125 \times\left(s-n_{\text {idlle }}\right)$. Higher values can be required by the manufacturer. |
| $\mathrm{m}_{\mathrm{t}}$ | kg | test mass of the vehicle |
| $\mathrm{ng}_{\text {max }}$ |  | number of foreward gears |
| ndv ${ }_{\text {i }}$ | $\min ^{-1} /(\mathrm{km} / \mathrm{h})$ | ratio of engine speed and vehicle speed for gear $\mathrm{i}, \mathrm{i}=1$ to $\mathrm{ng}_{\max }$ |
| $\mathrm{f}_{0}$ | N |  |
| $\mathrm{f}_{1}$ | N/(km/h) | driving resistance coefficients as defined in Annex 4 |
| $\mathrm{f}_{2}$ | $\mathrm{N} /(\mathrm{km} / \mathrm{h})^{2}$ |  |
| $\mathbf{P}_{\text {wot }}\left(\mathrm{n}_{\text {norm }}\right) / \mathrm{P}_{\text {rated }}$ |  | Normalised full load power curve as function of normalised engine speed $\mathrm{n}_{\text {norm }}=\left(\mathrm{n}-\mathrm{n}_{\text {idle }}\right) /\left(\mathrm{s}-\mathrm{n}_{\text {idle }}\right)$ |

### 5.3. Calculation steps

The calculation steps are described in the following paragraphs and summarized in Table 5-2.

## Calculation of required power

For every second j of the cycle trace the power required to overcome driving resistance and to accelerate is calculated using the following equation:

$$
\begin{equation*}
\left.P_{\text {required. } \mathrm{j}}=\left[\mathrm{f}_{0} \times \mathrm{v}_{\mathrm{j}}+\mathrm{f}_{1} \times\left(\mathrm{v}_{\mathrm{j}}\right)^{2}+\mathrm{f}_{2} \times\left(\mathrm{v}_{\mathrm{j}}\right)^{3}\right] / 3600+\left[\left(\mathrm{kr} \times \mathrm{a}_{\mathrm{j}}\right) \times \mathrm{v}_{\mathrm{j}} \times \mathrm{m}_{\mathrm{t}}\right)\right] / 3600 \tag{2}
\end{equation*}
$$

where:
$\mathrm{f}_{0}$ is the road load coefficient in N
$f_{1}$ is the road load parameter dependent on velocity in $N /(\mathrm{km} / \mathrm{h})$
$\mathrm{f}_{2}$ is the road load parameter based on the square of velocity in $\mathrm{N} /(\mathrm{km} / \mathrm{h})^{2}$
$P_{\text {required. } j}$ is the power required in kW at second j
$\mathrm{v}_{\mathrm{j}}$ is the vehicle speed at second j in $\mathrm{km} / \mathrm{h}$,
$a_{j}$ is the vehicle acceleration at second $j$ in $m / s^{2}, a_{j}=\left(v_{j+1}-v_{j}\right) / 3.6$
$\mathrm{m}_{\mathrm{t}}$ is the vehicle test mass in kg ,
kr is a factor taking the inertial resistances of the drivetrain during acceleration into account and is set to 1.1.

Determination of engine speeds

For each $\mathrm{v}_{\mathrm{j}} \leq 1 \mathrm{~km} / \mathrm{h}$, the engine speed is set to $\mathrm{n}_{\text {idle }}$ and the gear lever is placed in neutral with the clutch engaged.
For each $v_{j} \geq 1 \mathrm{~km} / \mathrm{h}$ of the cycle trace and each gear $\mathrm{i}, \mathrm{i}=1$ to $\mathrm{ng}_{\text {max }}$, the engine speed $\mathrm{n}_{\mathrm{i}, \mathrm{j}}$ is calculated using the following equation:

$$
\begin{equation*}
\mathrm{n}_{\mathrm{i}, \mathrm{j}}=\mathrm{ndv}_{\mathrm{i}} \times \mathrm{v}_{\mathrm{j}} \tag{3}
\end{equation*}
$$

All gears i for which $n_{\min } \leq n_{i, j} \leq n_{\text {max }}$ are possible gears to be used for driving the cycle trace at $v_{j}$.

$$
\begin{aligned}
\mathrm{n}_{\min } & =\mathrm{n}_{\text {min_drive }}, \text { if } \mathrm{i} \geq 3, \\
& =1.25 \times \mathrm{n}_{\text {idle }}, \text { if } \mathrm{i}=2, \\
& =\mathrm{n}_{\text {idle }} \text {, if } \mathrm{i}=1 \\
\mathrm{n}_{\max } & =0.9 \times\left(\mathrm{s}-\mathrm{n}_{\text {idle }}\right)+\mathrm{n}_{\text {idle }} .
\end{aligned}
$$

In cases where $\mathrm{v}_{\mathrm{j}}$ is $\geq 1 \mathrm{~km} / \mathrm{h}$ and $\mathrm{n}_{1, \mathrm{j}}$ drops below $\mathrm{n}_{\mathrm{idle}}$, the only possible gear is $\mathrm{ng}=1$ and the clutch must be disengaged.

Calculation of available power
The available power for each possible gear $i$ and each vehicle speed value of the cycle trace $v_{j}$ is calculated using the following equation:

$$
\begin{equation*}
\mathrm{P}_{\text {available }, \mathrm{i}, \mathrm{j}}=\mathrm{P}_{\text {norm_wot }}\left(\mathrm{n} \_ \text {norm }_{\mathrm{i}, \mathrm{j}}\right) \times \mathrm{P}_{\mathrm{n}} \times \mathrm{SM} \tag{4}
\end{equation*}
$$

where:
$\mathrm{n}_{\text {norm_ }} \mathrm{i}, \mathrm{j}=\left(\mathrm{ndv}_{\mathrm{i}} \times \mathrm{v}_{\mathrm{j}}-\mathrm{n}_{\text {idle }}\right) /\left(\mathrm{s}-\mathrm{n}_{\text {idle }}\right)$,
$P_{n}$ is the rated power in kW ,
$\mathrm{P}_{\text {norm_wot }}$ is the percentage of rated power available at $\mathrm{n}_{\text {norm_ } \mathrm{i}, \mathrm{j}}$ at full load condition from the normalized full load power curve,
SM is a safety margin accounting for the difference between stationary full load condition power curve and the power available during transient conditions. SM is set to 0.9 .
$\mathrm{n}_{\text {idle }}$ is the idling speed in $\mathrm{min}^{-1}$
$s$ is the rated engine speed, the engine speed in $\min ^{-1}$ at which an engine develops its maximum power. If the maximum power is developed over an engine speed range, $s$ is determined by the mean of this range.

Determination of possible gears to be used
The possible gears to be used are determined by:
(1) $\mathrm{n}_{\min } \leq \mathrm{n}_{\mathrm{i}, \mathrm{j}} \leq \mathrm{n}_{\max }$
as defined in paragraph 4.1.4 of this annex and
(2) $P_{\text {available, }, \mathrm{i}, \mathrm{j}} \geq P_{\text {required }, \mathrm{j}}$

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$\mathrm{P}_{\text {available, }, \mathrm{i}, \mathrm{j}}$ as defined in equation 2, $\mathrm{P}_{\mathrm{required}, \mathrm{j}}$ as defined equation 4 of this annex.

The initial gear to be used for each second j of the cycle trace is the maximum final possible gear i_max.

Table 5-2: Calculation steps

| Step | Task | Description/Requirements | Remark |
| :---: | :---: | :---: | :---: |
| 1 | Calculation of required power | $\begin{aligned} P_{\text {required }, j}= & {\left[f_{0} \times v_{j}+f_{1} \times\left(v_{j}\right)^{2}+f_{2} \times\left(v_{j}\right)^{3}\right] / 3600+} \\ & {\left.\left[\left(k r \times a_{j}\right) \times v_{j} \times m_{t}\right)\right] / 3600 } \end{aligned}$ | for each second $j$ of the cycle trace, $a_{j}$ is the vehicle acceleration, kr is a factor taking the inertial resistances of the drivetrain during acceleration into account and is set to 1.1 |
| 2 | Determination of engine speeds for each gear i | $\mathrm{n}_{\text {min }}=\mathrm{n}_{\text {min_drive }}$, if $\mathrm{i}>=3$, |  |
|  |  | $=1.25 \times \mathrm{n}_{\text {idlle }}$, if $\mathrm{i}=2$, |  |
|  |  | $=n_{\text {idle }}$, if $\mathrm{i}=1$ |  |
|  |  | $\mathrm{n}_{\max }=0.9 \times\left(\mathrm{s}-\mathrm{n}_{\text {idle }}\right)+\mathrm{n}_{\text {idle }}$. |  |
|  |  | $\mathrm{n}_{\text {min }}<=\mathrm{n}_{\mathrm{i}, \mathrm{j}}=\mathrm{ndv}_{\mathrm{i}} \times \mathrm{v}_{\mathrm{j}}<=\mathrm{n}_{\text {max }}$ |  |
| 3 | Calculation of available power | $\mathrm{P}_{\text {available }, \mathrm{i}, \mathrm{j}}=\mathrm{P}_{\text {norm_wot }}\left(\mathrm{n}_{\text {norm, }, \mathrm{i}, \mathrm{j}}\right) \times \mathrm{P}_{\text {rated }} \times \mathrm{SM}$ | SM is a safety margin accounting for the difference between stationary full load condition power curve and the power available during transient conditions. SM is set to 0.9. |
| 4 | Determination of possible gears to be used | The possible gears to be used are determined by |  |
|  |  | (1) $n_{\text {min }} \leq n_{i, j} \leq n_{\text {max }}$ as defined in paragraph 4.1.4 of this annex and |  |
|  |  | (2) $\mathrm{P}_{\text {available, }, \mathrm{j},} \geq \mathrm{P}_{\text {required, },}$ $\begin{aligned} & \mathrm{P}_{\text {available }, \mathrm{ij}} \text { as defined in paragraph } 4.1 .5 \text { of this annex, } \\ & \mathrm{P}_{\text {require, }, \mathrm{j}} \text { as defined in paragraph 4.1.3 of this annex } \\ & \hline \end{aligned}$ |  |
| 5 | Final gear choice | $\mathrm{i}_{\max }$ detemines the highest possible gear |  |

$j$ is the index for the cycle time, $i$ is the index for the gear number

### 5.4. Additional requirements for corrections and/or modifications of gear use

The initial gear use shall be checked and modified in order to avoid too frequent gearshifts and to ensure drivability and conformity with practical use. The requirements are described below and summarized in Table 5-3.
Corrections/modifications are made depending on the following requirements:
(a) First gear shall be selected 1 second before the beginning of an acceleration phase from standstill. Vehicle speeds below $1 \mathrm{~km} / \mathrm{h}$ imply that the vehicle is standing still.
(b) Skipping of gears during acceleration phases is not permitted. Gears used during accelerations and decelerations must be used for a period of at least 3 seconds.
E.g. a gear sequence $1,1,2,2,3,3,3,3,3$ is replaced by $1,1,1,2,2,2,3,3,3$
(c) Skipping of gears during deceleration phases is permitted. For the last phases of a deceleration down to a stop, the clutch may be either disengaged or the gear lever in neutral
position and the clutch engaged.
(d) There shall be no gearshift during the transition from an acceleration phase to a deceleration phase. E.g., if $v_{j}\left\langle v_{j+1}\right\rangle v_{j+2}$ and the gear for the time sequence $j$ and $j+1$ is $i$, gear $i$ is also kept for the time $\mathrm{j}+2$, even if the initial gear for $\mathrm{j}+2$ would be $\mathrm{i}+1$.
(e) If a gear i is used for a time sequence of 1 to 5 s and the gear before this sequence is the same as the gear after this sequence, e.g. i-1, the gear use for this sequence is corrected to i-1.
That means:
(1) a gear sequence $i-1, i, i-1$ is replaced by $i-1, i-1, i-1$
(2) a gear sequence $\mathrm{i}-1, \mathrm{i}, \mathrm{i}, \mathrm{i}-1$ is replaced by $\mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1$
(3) a gear sequence $i-1, i, i, i, i-1$ is replaced by $i-1, i-1, i-1, i-1, i-1$
(4) a gear sequence $i-1, i, i, i, i, i-1$ is replaced by $i-1, i-1, i-1, i-1, i-1, i-1$,
(5) a gear sequence $\mathrm{i}-1, \mathrm{i}, \mathrm{i}, \mathrm{i}, \mathrm{i}, \mathrm{i}, \mathrm{i}-1$ is replaced by $\mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1$.
for all cases (1) to (5), $\mathrm{g}_{\min } \leq \mathrm{i}$ must be fulfilled.
(f) a gear sequence $i, i-1, i$, is replaced by $i, i$, if the following conditions are fulfilled:
(1) the engine speed does not drop below $\mathrm{n}_{\text {min }}$ and
(2) These corrections do not occur more often than 4 times each for the low, medium and high speed cycle parts and not more than 3 times for the extra high speed part.

The requirement (2) is necessary, because the available power will drop below the required power, when the gear i-1 is replaced by i. And this should not occur too frequently.
(g) If during an acceleration phase a lower gear is required at a higher vehicle speed, the higher gears before are corrected to the lower gear, if the lower gear is required for at least 2 s .

Example: $\mathrm{vj}<\mathrm{vj}+1<\mathrm{vj}+2<\mathrm{vj}+3<\mathrm{vj}+4<\mathrm{vj}+5<\mathrm{vj}+6$. The originally calculated gear use is $2,3,3,3,2,2,3$. In this case the gear use will be corrected to $2,2,2,2,2,2,2,3$.
Since the above modifications may create new gear use sequences which are in conflict with these requirements, the gear sequences shall be checked twice.

Table 5-3: Additional requirements for corrections/modifications

| Step no | Step | Explanation |
| :---: | :---: | :---: |
| 1 | First gear shall be selected 1 second before the beginning of an acceleration phase from standstill. Vehicle speeds below $1 \mathrm{~km} / \mathrm{h}$ imply that the vehicle is standing still. |  |
| 2 | Skipping of gears during acceleration phases is not permitted. Gears used during accelerations and decelerations must be used for a period of at least 3 seconds. |  |
| 3 | Skipping of gears during deceleration phases is permitted. For the last phases of a deceleration down to stop, the clutch may be either disengaged or the gear lever in neutral position and the clutch engaged. |  |
| 4 | There shall be no gearshift during the transition from an acceleration phase to a deceleration phase. |  |
| 5 | If a gear $i$ is used for a time sequence of 1 to 5 s and the gear before this sequence is the same as the gear after this sequence, e.g. $\mathrm{i}-1$, the gear use for this sequence is corrected to $\mathrm{i}-1$. | $\begin{gathered} \mathrm{i}-1, \mathrm{i}, \mathrm{i}, \mathrm{i}, \mathrm{i}, \mathrm{i}, \mathrm{i}-1 \text { is replaced by } \\ \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1, \mathrm{i}-1 \end{gathered}$ |
| 6 | a gear sequence $i$, $i-1, i$, is replaced by $i, i, i$, if the following conditions are fulfilled: | The requirement (2) is necessary, because the available power will drop below the required power, when the gear $\mathrm{i}-1$ is replaced by i. And this should not occur too frequently. |
|  | (1) the engine speed does not drop below nmin and |  |
|  | (2) These corrections do not occur more often than 4 times each for the low, medium and high speed cycle parts and not more than 3 times for the extra high speed part. |  |
| 7 | If during an acceleration phase a lower gear is required at a higher vehicle speed, the higher gears before are corrected to the lower gear, if the lower gear is required for at least 2 s . | Example: The originally calculated gear use is $2,3,3,3$, $2,2,3$. In this case the gear use will be corrected to $2,2,2$, $2,2,2,2,3$. |

These modifications may create new gear sequences which are in conflict with these requirements, so the gear sequences shall be checked twice.

## 6. Summary and Conclusions

The development of a World-wide harmonized Light duty Test Cycle (WLTC) which will represent typical driving conditions around the world was presented. The driving cycle was obtained from recorded in-use data ("real world" data) from different regions of the world (EU, India, Japan, Korea, USA) combined with suitable weighting factors. Over $765,000 \mathrm{~km}$ of data was collected covering a wide range of vehicle categories (M1, N1 and M2 vehicles, various engine capacities, power-to-mass ratios, manufacturers etc), over different road types (urban, rural, motorway) and driving conditions (peak, off-peak, weekend). The WLTC contains four individual sections (Low, Medium, High and Extra-high speed phase), each one composed by a sequence of idles and short trips, and has a total duration of 1800 seconds. The length of each speed phase L/M/H/ExH phases is: 589 [s], 433 [s], 455 [s] and 323 [s] respectively.

The developed test cycle and the gearshift procedure were tested in several laboratories all over the world. The dynamics of the WLTC reflect the average driving behavior of light duty vehicle in real world. In addition to that, a good balance between representatively of in-use driving data and drivability on chassis dynamometer was also obtained.

The final result of the cycle development is as follows;

- For Class 1 vehicles: WLTC CL1 version 2.0
- For Class 1 vehicles: WLTC CL2 version 2.0
- For Class 3 vehicles of which maximum speed is less than $120 \mathrm{~km} / \mathrm{h}$ : WLTC CL3 version 5.1
- For Class 3 vehicles of which maximum speed is higher than $120 \mathrm{~km} / \mathrm{h}$ : WLTC CL3 version 5.3


## 7. Annex A - Final cycle time table (Class 1 ver.2.0, Class 2 ver.2.0, Class 3 Ver.5.1/5.3)

Table A/1
WLTC, Class 1 vehicles, phase Low

| Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 47 | 18.8 | 94 | 0 | 141 | 35.7 |
| 1 | 0 | 48 | 19.5 | 95 | 0 | 142 | 35.9 |
| 2 | 0 | 49 | 20.2 | 96 | 0 | 143 | 36.6 |
| 3 | 0 | 50 | 20.9 | 97 | 0 | 144 | 37.5 |
| 4 | 0 | 51 | 21.7 | 98 | 0 | 145 | 38.4 |
| 5 | 0 | 52 | 22.4 | 99 | 0 | 146 | 39.3 |
| 6 | 0 | 53 | 23.1 | 100 | 0 | 147 | 40 |
| 7 | 0 | 54 | 23.7 | 101 | 0 | 148 | 40.6 |
| 8 | 0 | 55 | 24.4 | 102 | 0 | 149 | 41.1 |
| 9 | 0 | 56 | 25.1 | 103 | 0 | 150 | 41.4 |
| 10 | 0 | 57 | 25.4 | 104 | 0 | 151 | 41.6 |
| 11 | 0 | 58 | 25.2 | 105 | 0 | 152 | 41.8 |
| 12 | 0.2 | 59 | 23.4 | 106 | 0 | 153 | 41.8 |
| 13 | 3.1 | 60 | 21.8 | 107 | 0 | 154 | 41.9 |
| 14 | 5.7 | 61 | 19.7 | 108 | 0.7 | 155 | 41.9 |
| 15 | 8 | 62 | 17.3 | 109 | 1.1 | 156 | 42 |
| 16 | 10.1 | 63 | 14.7 | 110 | 1.9 | 157 | 42 |
| 17 | 12 | 64 | 12 | 111 | 2.5 | 158 | 42.2 |
| 18 | 13.8 | 65 | 9.4 | 112 | 3.5 | 159 | 42.3 |
| 19 | 15.4 | 66 | 5.6 | 113 | 4.7 | 160 | 42.6 |
| 20 | 16.7 | 67 | 3.1 | 114 | 6.1 | 161 | 43 |
| 21 | 17.7 | 68 | 0 | 115 | 7.5 | 162 | 43.3 |
| 22 | 18.3 | 69 | 0 | 116 | 9.4 | 163 | 43.7 |
| 23 | 18.8 | 70 | 0 | 117 | 11 | 164 | 44 |
| 24 | 18.9 | 71 | 0 | 118 | 12.9 | 165 | 44.3 |
| 25 | 18.4 | 72 | 0 | 119 | 14.5 | 166 | 44.5 |
| 26 | 16.9 | 73 | 0 | 120 | 16.4 | 167 | 44.6 |
| 27 | 14.3 | 74 | 0 | 121 | 18 | 168 | 44.6 |
| 28 | 10.8 | 75 | 0 | 122 | 20 | 169 | 44.5 |
| 29 | 7.1 | 76 | 0 | 123 | 21.5 | 170 | 44.4 |
| 30 | 4 | 77 | 0 | 124 | 23.5 | 171 | 44.3 |
| 31 | 0 | 78 | 0 | 125 | 25 | 172 | 44.2 |
| 32 | 0 | 79 | 0 | 126 | 26.8 | 173 | 44.1 |
| 33 | 0 | 80 | 0 | 127 | 28.2 | 174 | 44 |
| 34 | 0 | 81 | 0 | 128 | 30 | 175 | 43.9 |
| 35 | 1.5 | 82 | 0 | 129 | 31.4 | 176 | 43.8 |
| 36 | 3.8 | 83 | 0 | 130 | 32.5 | 177 | 43.7 |
| 37 | 5.6 | 84 | 0 | 131 | 33.2 | 178 | 43.6 |
| 38 | 7.5 | 85 | 0 | 132 | 33.4 | 179 | 43.5 |
| 39 | 9.2 | 86 | 0 | 133 | 33.7 | 180 | 43.4 |
| 40 | 10.8 | 87 | 0 | 134 | 33.9 | 181 | 43.3 |
| 41 | 12.4 | 88 | 0 | 135 | 34.2 | 182 | 43.1 |
| 42 | 13.8 | 89 | 0 | 136 | 34.4 | 183 | 42.9 |
| 43 | 15.2 | 90 | 0 | 137 | 34.7 | 184 | 42.7 |
| 44 | 16.3 | 91 | 0 | 138 | 34.9 | 185 | 42.5 |
| 45 | 17.3 | 92 | 0 | 139 | 35.2 | 186 | 42.3 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 46 | 18 | 93 | 0 | 140 | 35.4 | 187 | 42.2 |


| Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 188 | 42.2 | 237 | 39.7 | 286 | 25.3 | 335 | 14.3 |
| 189 | 42.2 | 238 | 39.9 | 287 | 24.9 | 336 | 14.3 |
| 190 | 42.3 | 239 | 40 | 288 | 24.5 | 337 | 14 |
| 191 | 42.4 | 240 | 40.1 | 289 | 24.2 | 338 | 13 |
| 192 | 42.5 | 241 | 40.2 | 290 | 24 | 339 | 11.4 |
| 193 | 42.7 | 242 | 40.3 | 291 | 23.8 | 340 | 10.2 |
| 194 | 42.9 | 243 | 40.4 | 292 | 23.6 | 341 | 8 |
| 195 | 43.1 | 244 | 40.5 | 293 | 23.5 | 342 | 7 |
| 196 | 43.2 | 245 | 40.5 | 294 | 23.4 | 343 | 6 |
| 197 | 43.3 | 246 | 40.4 | 295 | 23.3 | 344 | 5.5 |
| 198 | 43.4 | 247 | 40.3 | 296 | 23.3 | 345 | 5 |
| 199 | 43.4 | 248 | 40.2 | 297 | 23.2 | 346 | 4.5 |
| 200 | 43.2 | 249 | 40.1 | 298 | 23.1 | 347 | 4 |
| 201 | 42.9 | 250 | 39.7 | 299 | 23 | 348 | 3.5 |
| 202 | 42.6 | 251 | 38.8 | 300 | 22.8 | 349 | 3 |
| 203 | 42.2 | 252 | 37.4 | 301 | 22.5 | 350 | 2.5 |
| 204 | 41.9 | 253 | 35.6 | 302 | 22.1 | 351 | 2 |
| 205 | 41.5 | 254 | 33.4 | 303 | 21.7 | 352 | 1.5 |
| 206 | 41 | 255 | 31.2 | 304 | 21.1 | 353 | 1 |
| 207 | 40.5 | 256 | 29.1 | 305 | 20.4 | 354 | 0.5 |
| 208 | 39.9 | 257 | 27.6 | 306 | 19.5 | 355 | 0 |
| 209 | 39.3 | 258 | 26.6 | 307 | 18.5 | 356 | 0 |
| 210 | 38.7 | 259 | 26.2 | 308 | 17.6 | 357 | 0 |
| 211 | 38.1 | 260 | 26.3 | 309 | 16.6 | 358 | 0 |
| 212 | 37.5 | 261 | 26.7 | 310 | 15.7 | 359 | 0 |
| 213 | 36.9 | 262 | 27.5 | 311 | 14.9 | 360 | 0 |
| 214 | 36.3 | 263 | 28.4 | 312 | 14.3 | 361 | 2.2 |
| 215 | 35.7 | 264 | 29.4 | 313 | 14.1 | 362 | 4.5 |
| 216 | 35.1 | 265 | 30.4 | 314 | 14 | 363 | 6.6 |
| 217 | 34.5 | 266 | 31.2 | 315 | 13.9 | 364 | 8.6 |
| 218 | 33.9 | 267 | 31.9 | 316 | 13.8 | 365 | 10.6 |
| 219 | 33.6 | 268 | 32.5 | 317 | 13.7 | 366 | 12.5 |
| 220 | 33.5 | 269 | 33 | 318 | 13.6 | 367 | 14.4 |
| 221 | 33.6 | 270 | 33.4 | 319 | 13.5 | 368 | 16.3 |
| 222 | 33.9 | 271 | 33.8 | 320 | 13.4 | 369 | 17.9 |
| 223 | 34.3 | 272 | 34.1 | 321 | 13.3 | 370 | 19.1 |
| 224 | 34.7 | 273 | 34.3 | 322 | 13.2 | 371 | 19.9 |
| 225 | 35.1 | 274 | 34.3 | 323 | 13.2 | 372 | 20.3 |
| 226 | 35.5 | 275 | 33.9 | 324 | 13.2 | 373 | 20.5 |
| 227 | 35.9 | 276 | 33.3 | 325 | 13.4 | 374 | 20.7 |
| 228 | 36.4 | 277 | 32.6 | 326 | 13.5 | 375 | 21 |
| 229 | 36.9 | 278 | 31.8 | 327 | 13.7 | 376 | 21.6 |
| 230 | 37.4 | 279 | 30.7 | 328 | 13.8 | 377 | 22.6 |
| 231 | 37.9 | 280 | 29.6 | 329 | 14 | 378 | 23.7 |
| 232 | 38.3 | 281 | 28.6 | 330 | 14.1 | 379 | 24.8 |
| 233 | 38.7 | 282 | 27.8 | 331 | 14.3 | 380 | 25.7 |
| 234 | 39.1 | 283 | 27 | 332 | 14.4 | 381 | 26.2 |
| 235 | 39.3 | 284 | 26.4 | 333 | 14.4 | 382 | 26.4 |
| 236 | 39.5 | 285 | 25.8 | 334 | 14.4 | 383 | 26.4 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 384 | 26.4 | 433 | 0 | 482 | 3.1 | 531 | 48.2 |
| 385 | 26.5 | 434 | 0 | 483 | 4.6 | 532 | 48.5 |
| 386 | 26.6 | 435 | 0 | 484 | 6.1 | 533 | 48.7 |
| 387 | 26.8 | 436 | 0 | 485 | 7.8 | 534 | 48.9 |
| 388 | 26.9 | 437 | 0 | 486 | 9.5 | 535 | 49.1 |
| 389 | 27.2 | 438 | 0 | 487 | 11.3 | 536 | 49.1 |
| 390 | 27.5 | 439 | 0 | 488 | 13.2 | 537 | 49 |
| 391 | 28 | 440 | 0 | 489 | 15 | 538 | 48.8 |
| 392 | 28.8 | 441 | 0 | 490 | 16.8 | 539 | 48.6 |
| 393 | 29.9 | 442 | 0 | 491 | 18.4 | 540 | 48.5 |
| 394 | 31 | 443 | 0 | 492 | 20.1 | 541 | 48.4 |
| 395 | 31.9 | 444 | 0 | 493 | 21.6 | 542 | 48.3 |
| 396 | 32.5 | 445 | 0 | 494 | 23.1 | 543 | 48.2 |
| 397 | 32.6 | 446 | 0 | 495 | 24.6 | 544 | 48.1 |
| 398 | 32.4 | 447 | 0 | 496 | 26 | 545 | 47.5 |
| 399 | 32 | 448 | 0 | 497 | 27.5 | 546 | 46.7 |
| 400 | 31.3 | 449 | 0 | 498 | 29 | 547 | 45.7 |
| 401 | 30.3 | 450 | 0 | 499 | 30.6 | 548 | 44.6 |
| 402 | 28 | 451 | 0 | 500 | 32.1 | 549 | 42.9 |
| 403 | 27 | 452 | 0 | 501 | 33.7 | 550 | 40.8 |
| 404 | 24 | 453 | 0 | 502 | 35.3 | 551 | 38.2 |
| 405 | 22.5 | 454 | 0 | 503 | 36.8 | 552 | 35.3 |
| 406 | 19 | 455 | 0 | 504 | 38.1 | 553 | 31.8 |
| 407 | 17.5 | 456 | 0 | 505 | 39.3 | 554 | 28.7 |
| 408 | 14 | 457 | 0 | 506 | 40.4 | 555 | 25.8 |
| 409 | 12.5 | 458 | 0 | 507 | 41.2 | 556 | 22.9 |
| 410 | 9 | 459 | 0 | 508 | 41.9 | 557 | 20.2 |
| 411 | 7.5 | 460 | 0 | 509 | 42.6 | 558 | 17.3 |
| 412 | 4 | 461 | 0 | 510 | 43.3 | 559 | 15 |
| 413 | 2.9 | 462 | 0 | 511 | 44 | 560 | 12.3 |
| 414 | 0 | 463 | 0 | 512 | 44.6 | 561 | 10.3 |
| 415 | 0 | 464 | 0 | 513 | 45.3 | 562 | 7.8 |
| 416 | 0 | 465 | 0 | 514 | 45.5 | 563 | 6.5 |
| 417 | 0 | 466 | 0 | 515 | 45.5 | 564 | 4.4 |
| 418 | 0 | 467 | 0 | 516 | 45.2 | 565 | 3.2 |
| 419 | 0 | 468 | 0 | 517 | 44.7 | 566 | 1.2 |
| 420 | 0 | 469 | 0 | 518 | 44.2 | 567 | 0 |
| 421 | 0 | 470 | 0 | 519 | 43.6 | 568 | 0 |
| 422 | 0 | 471 | 0 | 520 | 43.1 | 569 | 0 |
| 423 | 0 | 472 | 0 | 521 | 42.8 | 570 | 0 |
| 424 | 0 | 473 | 0 | 522 | 42.7 | 571 | 0 |
| 425 | 0 | 474 | 0 | 523 | 42.8 | 572 | 0 |
| 426 | 0 | 475 | 0 | 524 | 43.3 | 573 | 0 |
| 427 | 0 | 476 | 0 | 525 | 43.9 | 574 | 0 |
| 428 | 0 | 477 | 0 | 526 | 44.6 | 575 | 0 |
| 429 | 0 | 478 | 0 | 527 | 45.4 | 576 | 0 |
| 430 | 0 | 479 | 0 | 528 | 46.3 | 577 | 0 |
| 431 | 0 | 480 | 0 | 529 | 47.2 | 578 | 0 |
| 432 | 0 | 481 | 1.6 | 530 | 47.8 | 579 | 0 |

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| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| speed in $\mathrm{km} / \mathrm{h}$ |  |  |  |  |  |  |
| 580 | 0 |  |  |  |  |  |
| 581 | 0 |  |  |  |  |  |
| 582 | 0 |  |  |  |  |  |
| 583 | 0 |  |  |  |  |  |
| 584 | 0 |  |  |  |  |  |
| 585 | 0 |  |  |  |  |  |
| 586 | 0 |  |  |  |  |  |
| 587 | 0 |  |  |  |  |  |
| 588 | 0 |  |  |  |  |  |
| 589 | 0 |  |  |  |  |  |

Table A/2
WLTC, Class 1 vehicles, phase Medium

| Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 590 | 0 | 637 | 18.4 | 684 | 56.2 | 731 | 57.9 |
| 591 | 0 | 638 | 19 | 685 | 56.7 | 732 | 58.8 |
| 592 | 0 | 639 | 20.1 | 686 | 57.3 | 733 | 59.6 |
| 593 | 0 | 640 | 21.5 | 687 | 57.9 | 734 | 60.3 |
| 594 | 0 | 641 | 23.1 | 688 | 58.4 | 735 | 60.9 |
| 595 | 0 | 642 | 24.9 | 689 | 58.8 | 736 | 61.3 |
| 596 | 0 | 643 | 26.4 | 690 | 58.9 | 737 | 61.7 |
| 597 | 0 | 644 | 27.9 | 691 | 58.4 | 738 | 61.8 |
| 598 | 0 | 645 | 29.2 | 692 | 58.1 | 739 | 61.8 |
| 599 | 0 | 646 | 30.4 | 693 | 57.6 | 740 | 61.6 |
| 600 | 0.6 | 647 | 31.6 | 694 | 56.9 | 741 | 61.2 |
| 601 | 1.9 | 648 | 32.8 | 695 | 56.3 | 742 | 60.8 |
| 602 | 2.7 | 649 | 34 | 696 | 55.7 | 743 | 60.4 |
| 603 | 5.2 | 650 | 35.1 | 697 | 55.3 | 744 | 59.9 |
| 604 | 7 | 651 | 36.3 | 698 | 55 | 745 | 59.4 |
| 605 | 9.6 | 652 | 37.4 | 699 | 54.7 | 746 | 58.9 |
| 606 | 11.4 | 653 | 38.6 | 700 | 54.5 | 747 | 58.6 |
| 607 | 14.1 | 654 | 39.6 | 701 | 54.4 | 748 | 58.2 |
| 608 | 15.8 | 655 | 40.6 | 702 | 54.3 | 749 | 57.9 |
| 609 | 18.2 | 656 | 41.6 | 703 | 54.2 | 750 | 57.7 |
| 610 | 19.7 | 657 | 42.4 | 704 | 54.1 | 751 | 57.5 |
| 611 | 21.8 | 658 | 43 | 705 | 53.8 | 752 | 57.2 |
| 612 | 23.2 | 659 | 43.6 | 706 | 53.5 | 753 | 57 |
| 613 | 24.7 | 660 | 44 | 707 | 53 | 754 | 56.8 |
| 614 | 25.8 | 661 | 44.4 | 708 | 52.6 | 755 | 56.6 |
| 615 | 26.7 | 662 | 44.8 | 709 | 52.2 | 756 | 56.6 |
| 616 | 27.2 | 663 | 45.2 | 710 | 51.9 | 757 | 56.7 |
| 617 | 27.7 | 664 | 45.6 | 711 | 51.7 | 758 | 57.1 |
| 618 | 28.1 | 665 | 46 | 712 | 51.7 | 759 | 57.6 |
| 619 | 28.4 | 666 | 46.5 | 713 | 51.8 | 760 | 58.2 |
| 620 | 28.7 | 667 | 47 | 714 | 52 | 761 | 59 |
| 621 | 29 | 668 | 47.5 | 715 | 52.3 | 762 | 59.8 |
| 622 | 29.2 | 669 | 48 | 716 | 52.6 | 763 | 60.6 |
| 623 | 29.4 | 670 | 48.6 | 717 | 52.9 | 764 | 61.4 |
| 624 | 29.4 | 671 | 49.1 | 718 | 53.1 | 765 | 62.2 |
| 625 | 29.3 | 672 | 49.7 | 719 | 53.2 | 766 | 62.9 |
| 626 | 28.9 | 673 | 50.2 | 720 | 53.3 | 767 | 63.5 |
| 627 | 28.5 | 674 | 50.8 | 721 | 53.3 | 768 | 64.2 |
| 628 | 28.1 | 675 | 51.3 | 722 | 53.4 | 769 | 64.4 |
| 629 | 27.6 | 676 | 51.8 | 723 | 53.5 | 770 | 64.4 |
| 630 | 26.9 | 677 | 52.3 | 724 | 53.7 | 771 | 64 |
| 631 | 26 | 678 | 52.9 | 725 | 54 | 772 | 63.5 |
| 632 | 24.6 | 679 | 53.4 | 726 | 54.4 | 773 | 62.9 |
| 633 | 22.8 | 680 | 54 | 727 | 54.9 | 774 | 62.4 |
| 634 | 21 | 681 | 54.5 | 728 | 55.6 | 775 | 62 |
| 635 | 19.5 | 682 | 55.1 | 729 | 56.3 | 776 | 61.6 |
| 636 | 18.6 | 683 | 55.6 | 730 | 57.1 | 777 | 61.4 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 778 | 61.2 | 827 | 49.7 | 876 | 53.2 | 925 | 44.4 |
| 779 | 61 | 828 | 50.6 | 877 | 53.1 | 926 | 44.5 |
| 780 | 60.7 | 829 | 51.6 | 878 | 53 | 927 | 44.6 |
| 781 | 60.2 | 830 | 52.5 | 879 | 53 | 928 | 44.7 |
| 782 | 59.6 | 831 | 53.3 | 880 | 53 | 929 | 44.6 |
| 783 | 58.9 | 832 | 54.1 | 881 | 53 | 930 | 44.5 |
| 784 | 58.1 | 833 | 54.7 | 882 | 53 | 931 | 44.4 |
| 785 | 57.2 | 834 | 55.3 | 883 | 53 | 932 | 44.2 |
| 786 | 56.3 | 835 | 55.7 | 884 | 52.8 | 933 | 44.1 |
| 787 | 55.3 | 836 | 56.1 | 885 | 52.5 | 934 | 43.7 |
| 788 | 54.4 | 837 | 56.4 | 886 | 51.9 | 935 | 43.3 |
| 789 | 53.4 | 838 | 56.7 | 887 | 51.1 | 936 | 42.8 |
| 790 | 52.4 | 839 | 57.1 | 888 | 50.2 | 937 | 42.3 |
| 791 | 51.4 | 840 | 57.5 | 889 | 49.2 | 938 | 41.6 |
| 792 | 50.4 | 841 | 58 | 890 | 48.2 | 939 | 40.7 |
| 793 | 49.4 | 842 | 58.7 | 891 | 47.3 | 940 | 39.8 |
| 794 | 48.5 | 843 | 59.3 | 892 | 46.4 | 941 | 38.8 |
| 795 | 47.5 | 844 | 60 | 893 | 45.6 | 942 | 37.8 |
| 796 | 46.5 | 845 | 60.6 | 894 | 45 | 943 | 36.9 |
| 797 | 45.4 | 846 | 61.3 | 895 | 44.3 | 944 | 36.1 |
| 798 | 44.3 | 847 | 61.5 | 896 | 43.8 | 945 | 35.5 |
| 799 | 43.1 | 848 | 61.5 | 897 | 43.3 | 946 | 35 |
| 800 | 42 | 849 | 61.4 | 898 | 42.8 | 947 | 34.7 |
| 801 | 40.8 | 850 | 61.2 | 899 | 42.4 | 948 | 34.4 |
| 802 | 39.7 | 851 | 60.5 | 900 | 42 | 949 | 34.1 |
| 803 | 38.8 | 852 | 60 | 901 | 41.6 | 950 | 33.9 |
| 804 | 38.1 | 853 | 59.5 | 902 | 41.1 | 951 | 33.6 |
| 805 | 37.4 | 854 | 58.9 | 903 | 40.3 | 952 | 33.3 |
| 806 | 37.1 | 855 | 58.4 | 904 | 39.5 | 953 | 33 |
| 807 | 36.9 | 856 | 57.9 | 905 | 38.6 | 954 | 32.7 |
| 808 | 37 | 857 | 57.5 | 906 | 37.7 | 955 | 32.3 |
| 809 | 37.5 | 858 | 57.1 | 907 | 36.7 | 956 | 31.9 |
| 810 | 37.8 | 859 | 56.7 | 908 | 36.2 | 957 | 31.5 |
| 811 | 38.2 | 860 | 56.4 | 909 | 36 | 958 | 31 |
| 812 | 38.6 | 861 | 56.1 | 910 | 36.2 | 959 | 30.6 |
| 813 | 39.1 | 862 | 55.8 | 911 | 37 | 960 | 30.2 |
| 814 | 39.6 | 863 | 55.5 | 912 | 38 | 961 | 29.7 |
| 815 | 40.1 | 864 | 55.3 | 913 | 39 | 962 | 29.1 |
| 816 | 40.7 | 865 | 55 | 914 | 39.7 | 963 | 28.4 |
| 817 | 41.3 | 866 | 54.7 | 915 | 40.2 | 964 | 27.6 |
| 818 | 41.9 | 867 | 54.4 | 916 | 40.7 | 965 | 26.8 |
| 819 | 42.7 | 868 | 54.2 | 917 | 41.2 | 966 | 26 |
| 820 | 43.4 | 869 | 54 | 918 | 41.7 | 967 | 25.1 |
| 821 | 44.2 | 870 | 53.9 | 919 | 42.2 | 968 | 24.2 |
| 822 | 45 | 871 | 53.7 | 920 | 42.7 | 969 | 23.3 |
| 823 | 45.9 | 872 | 53.6 | 921 | 43.2 | 970 | 22.4 |
| 824 | 46.8 | 873 | 53.5 | 922 | 43.6 | 971 | 21.5 |
| 825 | 47.7 | 874 | 53.4 | 923 | 44 | 972 | 20.6 |
| 826 | 48.7 | 875 | 53.3 | 924 | 44.2 | 973 | 19.7 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 974 | 18.8 |  |  |  |  |  |  |
| 975 | 17.7 |  |  |  |  |  |  |
| 976 | 16.4 |  |  |  |  |  |  |
| 977 | 14.9 |  |  |  |  |  |  |
| 978 | 13.2 |  |  |  |  |  |  |
| 979 | 11.3 |  |  |  |  |  |  |
| 980 | 9.4 |  |  |  |  |  |  |
| 981 | 7.5 |  |  |  |  |  |  |
| 982 | 5.6 |  |  |  |  |  |  |
| 983 | 3.7 |  |  |  |  |  |  |
| 984 | 1.9 |  |  |  |  |  |  |
| 985 | 1 |  |  |  |  |  |  |
| 986 | 0 |  |  |  |  |  |  |
| 987 | 0 |  |  |  |  |  |  |
| 988 | 0 |  |  |  |  |  |  |
| 989 | 0 |  |  |  |  |  |  |
| 990 | 0 |  |  |  |  |  |  |
| 991 | 0 |  |  |  |  |  |  |
| 992 | 0 |  |  |  |  |  |  |
| 993 | 0 |  |  |  |  |  |  |
| 994 | 0 |  |  |  |  |  |  |
| 995 | 0 |  |  |  |  |  |  |
| 996 | 0 |  |  |  |  |  |  |
| 997 | 0 |  |  |  |  |  |  |
| 998 | 0 |  |  |  |  |  |  |
| 999 | 0 |  |  |  |  |  |  |
| 1000 | 0 |  |  |  |  |  |  |
| 1001 | 0 |  |  |  |  |  |  |
| 1002 | 0 |  |  |  |  |  |  |
| 1003 | 0 |  |  |  |  |  |  |
| 1004 | 0 |  |  |  |  |  |  |
| 1005 | 0 |  |  |  |  |  |  |
| 1006 | 0 |  |  |  |  |  |  |
| 1007 | 0 |  |  |  |  |  |  |
| 1008 | 0 |  |  |  |  |  |  |
| 1009 | 0 |  |  |  |  |  |  |
| 1010 | 0 |  |  |  |  |  |  |
| 1011 | 0 |  |  |  |  |  |  |
| 1012 | 0 |  |  |  |  |  |  |
| 1013 | 0 |  |  |  |  |  |  |
| 1014 | 0 |  |  |  |  |  |  |
| 1015 | 0 |  |  |  |  |  |  |
| 1016 | 0 |  |  |  |  |  |  |
| 1017 | 0 |  |  |  |  |  |  |
| 1018 | 0 |  |  |  |  |  |  |
| 1019 | 0 |  |  |  |  |  |  |
| 1020 | 0 |  |  |  |  |  |  |
| 1021 | 0 |  |  |  |  |  |  |
| 1022 | 0 |  |  |  |  |  |  |

Table A/3
WLTC, Class 2 vehicles, phase Low

| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 47 | 11.6 | 94 | 0 | 141 | 36.8 |
| 1 | 0 | 48 | 12.4 | 95 | 0 | 142 | 35.1 |
| 2 | 0 | 49 | 13.2 | 96 | 0 | 143 | 32.2 |
| 3 | 0 | 50 | 14.2 | 97 | 0 | 144 | 31.1 |
| 4 | 0 | 51 | 14.8 | 98 | 0 | 145 | 30.8 |
| 5 | 0 | 52 | 14.7 | 99 | 0 | 146 | 29.7 |
| 6 | 0 | 53 | 14.4 | 100 | 0 | 147 | 29.4 |
| 7 | 0 | 54 | 14.1 | 101 | 0 | 148 | 29 |
| 8 | 0 | 55 | 13.6 | 102 | 0 | 149 | 28.5 |
| 9 | 0 | 56 | 13 | 103 | 0 | 150 | 26 |
| 10 | 0 | 57 | 12.4 | 104 | 0 | 151 | 23.4 |
| 11 | 0 | 58 | 11.8 | 105 | 0 | 152 | 20.7 |
| 12 | 0 | 59 | 11.2 | 106 | 0 | 153 | 17.4 |
| 13 | 1.2 | 60 | 10.6 | 107 | 0.8 | 154 | 15.2 |
| 14 | 2.6 | 61 | 9.9 | 108 | 1.4 | 155 | 13.5 |
| 15 | 4.9 | 62 | 9 | 109 | 2.3 | 156 | 13 |
| 16 | 7.3 | 63 | 8.2 | 110 | 3.5 | 157 | 12.4 |
| 17 | 9.4 | 64 | 7 | 111 | 4.7 | 158 | 12.3 |
| 18 | 11.4 | 65 | 4.8 | 112 | 5.9 | 159 | 12.2 |
| 19 | 12.7 | 66 | 2.3 | 113 | 7.4 | 160 | 12.3 |
| 20 | 13.3 | 67 | 0 | 114 | 9.2 | 161 | 12.4 |
| 21 | 13.4 | 68 | 0 | 115 | 11.7 | 162 | 12.5 |
| 22 | 13.3 | 69 | 0 | 116 | 13.5 | 163 | 12.7 |
| 23 | 13.1 | 70 | 0 | 117 | 15 | 164 | 12.8 |
| 24 | 12.5 | 71 | 0 | 118 | 16.2 | 165 | 13.2 |
| 25 | 11.1 | 72 | 0 | 119 | 16.8 | 166 | 14.3 |
| 26 | 8.9 | 73 | 0 | 120 | 17.5 | 167 | 16.5 |
| 27 | 6.2 | 74 | 0 | 121 | 18.8 | 168 | 19.4 |
| 28 | 3.8 | 75 | 0 | 122 | 20.3 | 169 | 21.7 |
| 29 | 1.8 | 76 | 0 | 123 | 22 | 170 | 23.1 |
| 30 | 0 | 77 | 0 | 124 | 23.6 | 171 | 23.5 |
| 31 | 0 | 78 | 0 | 125 | 24.8 | 172 | 24.2 |
| 32 | 0 | 79 | 0 | 126 | 25.6 | 173 | 24.8 |
| 33 | 0 | 80 | 0 | 127 | 26.3 | 174 | 25.4 |
| 34 | 1.5 | 81 | 0 | 128 | 27.2 | 175 | 25.8 |
| 35 | 2.8 | 82 | 0 | 129 | 28.3 | 176 | 26.5 |
| 36 | 3.6 | 83 | 0 | 130 | 29.6 | 177 | 27.2 |
| 37 | 4.5 | 84 | 0 | 131 | 30.9 | 178 | 28.3 |
| 38 | 5.3 | 85 | 0 | 132 | 32.2 | 179 | 29.9 |
| 39 | 6 | 86 | 0 | 133 | 33.4 | 180 | 32.4 |
| 40 | 6.6 | 87 | 0 | 134 | 35.1 | 181 | 35.1 |
| 41 | 7.3 | 88 | 0 | 135 | 37.2 | 182 | 37.5 |
| 42 | 7.9 | 89 | 0 | 136 | 38.7 | 183 | 39.2 |
| 43 | 8.6 | 90 | 0 | 137 | 39 | 184 | 40.5 |
| 44 | 9.3 | 91 | 0 | 138 | 40.1 | 185 | 41.4 |
| 45 | 10 | 92 | 0 | 139 | 40.4 | 186 | 42 |
| 46 | 10.8 | 93 | 0 | 140 | 39.7 | 187 | 42.5 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 188 | 43.2 | 237 | 33.5 | 286 | 32.5 | 335 | 25 |
| 189 | 44.4 | 238 | 35.8 | 287 | 30.9 | 336 | 24.6 |
| 190 | 45.9 | 239 | 37.6 | 288 | 28.6 | 337 | 23.9 |
| 191 | 47.6 | 240 | 38.8 | 289 | 25.9 | 338 | 23 |
| 192 | 49 | 241 | 39.6 | 290 | 23.1 | 339 | 21.8 |
| 193 | 50 | 242 | 40.1 | 291 | 20.1 | 340 | 20.7 |
| 194 | 50.2 | 243 | 40.9 | 292 | 17.3 | 341 | 19.6 |
| 195 | 50.1 | 244 | 41.8 | 293 | 15.1 | 342 | 18.7 |
| 196 | 49.8 | 245 | 43.3 | 294 | 13.7 | 343 | 18.1 |
| 197 | 49.4 | 246 | 44.7 | 295 | 13.4 | 344 | 17.5 |
| 198 | 48.9 | 247 | 46.4 | 296 | 13.9 | 345 | 16.7 |
| 199 | 48.5 | 248 | 47.9 | 297 | 15 | 346 | 15.4 |
| 200 | 48.3 | 249 | 49.6 | 298 | 16.3 | 347 | 13.6 |
| 201 | 48.2 | 250 | 49.6 | 299 | 17.4 | 348 | 11.2 |
| 202 | 47.9 | 251 | 48.8 | 300 | 18.2 | 349 | 8.6 |
| 203 | 47.1 | 252 | 48 | 301 | 18.6 | 350 | 6 |
| 204 | 45.5 | 253 | 47.5 | 302 | 19 | 351 | 3.1 |
| 205 | 43.2 | 254 | 47.1 | 303 | 19.4 | 352 | 1.2 |
| 206 | 40.6 | 255 | 46.9 | 304 | 19.8 | 353 | 0 |
| 207 | 38.5 | 256 | 45.8 | 305 | 20.1 | 354 | 0 |
| 208 | 36.9 | 257 | 45.8 | 306 | 20.5 | 355 | 0 |
| 209 | 35.9 | 258 | 45.8 | 307 | 20.2 | 356 | 0 |
| 210 | 35.3 | 259 | 45.9 | 308 | 18.6 | 357 | 0 |
| 211 | 34.8 | 260 | 46.2 | 309 | 16.5 | 358 | 0 |
| 212 | 34.5 | 261 | 46.4 | 310 | 14.4 | 359 | 0 |
| 213 | 34.2 | 262 | 46.6 | 311 | 13.4 | 360 | 1.4 |
| 214 | 34 | 263 | 46.8 | 312 | 12.9 | 361 | 3.2 |
| 215 | 33.8 | 264 | 47 | 313 | 12.7 | 362 | 5.6 |
| 216 | 33.6 | 265 | 47.3 | 314 | 12.4 | 363 | 8.1 |
| 217 | 33.5 | 266 | 47.5 | 315 | 12.4 | 364 | 10.3 |
| 218 | 33.5 | 267 | 47.9 | 316 | 12.8 | 365 | 12.1 |
| 219 | 33.4 | 268 | 48.3 | 317 | 14.1 | 366 | 12.6 |
| 220 | 33.3 | 269 | 48.3 | 318 | 16.2 | 367 | 13.6 |
| 221 | 33.3 | 270 | 48.2 | 319 | 18.8 | 368 | 14.5 |
| 222 | 33.2 | 271 | 48 | 320 | 21.9 | 369 | 15.6 |
| 223 | 33.1 | 272 | 47.7 | 321 | 25 | 370 | 16.8 |
| 224 | 33 | 273 | 47.2 | 322 | 28.4 | 371 | 18.2 |
| 225 | 32.9 | 274 | 46.5 | 323 | 31.3 | 372 | 19.6 |
| 226 | 32.8 | 275 | 45.2 | 324 | 34 | 373 | 20.9 |
| 227 | 32.7 | 276 | 43.7 | 325 | 34.6 | 374 | 22.3 |
| 228 | 32.5 | 277 | 42 | 326 | 33.9 | 375 | 23.8 |
| 229 | 32.3 | 278 | 40.4 | 327 | 31.9 | 376 | 25.4 |
| 230 | 31.8 | 279 | 39 | 328 | 30 | 377 | 27 |
| 231 | 31.4 | 280 | 37.7 | 329 | 29 | 378 | 28.6 |
| 232 | 30.9 | 281 | 36.4 | 330 | 27.9 | 379 | 30.2 |
| 233 | 30.6 | 282 | 35.2 | 331 | 27.1 | 380 | 31.2 |
| 234 | 30.6 | 283 | 34.3 | 332 | 26.4 | 381 | 31.2 |
| 235 | 30.7 | 284 | 33.8 | 333 | 25.9 | 382 | 30.7 |
| 236 | 32 | 285 | 33.3 | 334 | 25.5 | 383 | 29.5 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 384 | 28.6 | 433 | 0 | 482 | 2.5 | 531 | 26 |
| 385 | 27.7 | 434 | 0 | 483 | 5.2 | 532 | 26.5 |
| 386 | 26.9 | 435 | 0 | 484 | 7.9 | 533 | 26.9 |
| 387 | 26.1 | 436 | 0 | 485 | 10.3 | 534 | 27.3 |
| 388 | 25.4 | 437 | 0 | 486 | 12.7 | 535 | 27.9 |
| 389 | 24.6 | 438 | 0 | 487 | 15 | 536 | 30.3 |
| 390 | 23.6 | 439 | 0 | 488 | 17.4 | 537 | 33.2 |
| 391 | 22.6 | 440 | 0 | 489 | 19.7 | 538 | 35.4 |
| 392 | 21.7 | 441 | 0 | 490 | 21.9 | 539 | 38 |
| 393 | 20.7 | 442 | 0 | 491 | 24.1 | 540 | 40.1 |
| 394 | 19.8 | 443 | 0 | 492 | 26.2 | 541 | 42.7 |
| 395 | 18.8 | 444 | 0 | 493 | 28.1 | 542 | 44.5 |
| 396 | 17.7 | 445 | 0 | 494 | 29.7 | 543 | 46.3 |
| 397 | 16.6 | 446 | 0 | 495 | 31.3 | 544 | 47.6 |
| 398 | 15.6 | 447 | 0 | 496 | 33 | 545 | 48.8 |
| 399 | 14.8 | 448 | 0 | 497 | 34.7 | 546 | 49.7 |
| 400 | 14.3 | 449 | 0 | 498 | 36.3 | 547 | 50.6 |
| 401 | 13.8 | 450 | 0 | 499 | 38.1 | 548 | 51.4 |
| 402 | 13.4 | 451 | 0 | 500 | 39.4 | 549 | 51.4 |
| 403 | 13.1 | 452 | 0 | 501 | 40.4 | 550 | 50.2 |
| 404 | 12.8 | 453 | 0 | 502 | 41.2 | 551 | 47.1 |
| 405 | 12.3 | 454 | 0 | 503 | 42.1 | 552 | 44.5 |
| 406 | 11.6 | 455 | 0 | 504 | 43.2 | 553 | 41.5 |
| 407 | 10.5 | 456 | 0 | 505 | 44.3 | 554 | 38.5 |
| 408 | 9 | 457 | 0 | 506 | 45.7 | 555 | 35.5 |
| 409 | 7.2 | 458 | 0 | 507 | 45.4 | 556 | 32.5 |
| 410 | 5.2 | 459 | 0 | 508 | 44.5 | 557 | 29.5 |
| 411 | 2.9 | 460 | 0 | 509 | 42.5 | 558 | 26.5 |
| 412 | 1.2 | 461 | 0 | 510 | 39.5 | 559 | 23.5 |
| 413 | 0 | 462 | 0 | 511 | 36.5 | 560 | 20.4 |
| 414 | 0 | 463 | 0 | 512 | 33.5 | 561 | 17.5 |
| 415 | 0 | 464 | 0 | 513 | 30.4 | 562 | 14.5 |
| 416 | 0 | 465 | 0 | 514 | 27 | 563 | 11.5 |
| 417 | 0 | 466 | 0 | 515 | 23.6 | 564 | 8.5 |
| 418 | 0 | 467 | 0 | 516 | 21 | 565 | 5.6 |
| 419 | 0 | 468 | 0 | 517 | 19.5 | 566 | 2.6 |
| 420 | 0 | 469 | 0 | 518 | 17.6 | 567 | 0 |
| 421 | 0 | 470 | 0 | 519 | 16.1 | 568 | 0 |
| 422 | 0 | 471 | 0 | 520 | 14.5 | 569 | 0 |
| 423 | 0 | 472 | 0 | 521 | 13.5 | 570 | 0 |
| 424 | 0 | 473 | 0 | 522 | 13.7 | 571 | 0 |
| 425 | 0 | 474 | 0 | 523 | 16 | 572 | 0 |
| 426 | 0 | 475 | 0 | 524 | 18.1 | 573 | 0 |
| 427 | 0 | 476 | 0 | 525 | 20.8 | 574 | 0 |
| 428 | 0 | 477 | 0 | 526 | 21.5 | 575 | 0 |
| 429 | 0 | 478 | 0 | 527 | 22.5 | 576 | 0 |
| 430 | 0 | 479 | 0 | 528 | 23.4 | 577 | 0 |
| 431 | 0 | 480 | 0 | 529 | 24.5 | 578 | 0 |
| 432 | 0 | 481 | 1.4 | 530 | 25.6 | 579 | 0 |

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| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| speed in $\mathrm{km} / \mathrm{h}$ |  |  |  |  |  |  |
| 580 | 0 |  |  |  |  |  |
| 581 | 0 |  |  |  |  |  |
| 582 | 0 |  |  |  |  |  |
| 583 | 0 |  |  |  |  |  |
| 584 | 0 |  |  |  |  |  |
| 585 | 0 |  |  |  |  |  |
| 586 | 0 |  |  |  |  |  |
| 587 | 0 |  |  |  |  |  |
| 588 | 0 |  |  |  |  |  |
| 589 | 0 |  |  |  |  |  |

Table A/4
WLTC, Class 2 vehicles, phase Medium

| Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 590 | 0 | 637 | 38.6 | 684 | 59.3 | 731 | 55.3 |
| 591 | 0 | 638 | 39.8 | 685 | 60.2 | 732 | 55.1 |
| 592 | 0 | 639 | 40.6 | 686 | 61.3 | 733 | 54.8 |
| 593 | 0 | 640 | 41.1 | 687 | 62.4 | 734 | 54.6 |
| 594 | 0 | 641 | 41.9 | 688 | 63.4 | 735 | 54.5 |
| 595 | 0 | 642 | 42.8 | 689 | 64.4 | 736 | 54.3 |
| 596 | 0 | 643 | 44.3 | 690 | 65.4 | 737 | 53.9 |
| 597 | 0 | 644 | 45.7 | 691 | 66.3 | 738 | 53.4 |
| 598 | 0 | 645 | 47.4 | 692 | 67.2 | 739 | 52.6 |
| 599 | 0 | 646 | 48.9 | 693 | 68 | 740 | 51.5 |
| 600 | 0 | 647 | 50.6 | 694 | 68.8 | 741 | 50.2 |
| 601 | 1.6 | 648 | 52 | 695 | 69.5 | 742 | 48.7 |
| 602 | 3.6 | 649 | 53.7 | 696 | 70.1 | 743 | 47 |
| 603 | 6.3 | 650 | 55 | 697 | 70.6 | 744 | 45.1 |
| 604 | 9 | 651 | 56.8 | 698 | 71 | 745 | 43 |
| 605 | 11.8 | 652 | 58 | 699 | 71.6 | 746 | 40.6 |
| 606 | 14.2 | 653 | 59.8 | 700 | 72.2 | 747 | 38.1 |
| 607 | 16.6 | 654 | 61.1 | 701 | 72.8 | 748 | 35.4 |
| 608 | 18.5 | 655 | 62.4 | 702 | 73.5 | 749 | 32.7 |
| 609 | 20.8 | 656 | 63 | 703 | 74.1 | 750 | 30 |
| 610 | 23.4 | 657 | 63.5 | 704 | 74.3 | 751 | 27.5 |
| 611 | 26.9 | 658 | 63 | 705 | 74.3 | 752 | 25.3 |
| 612 | 30.3 | 659 | 62 | 706 | 73.7 | 753 | 23.4 |
| 613 | 32.8 | 660 | 60.4 | 707 | 71.9 | 754 | 22 |
| 614 | 34.1 | 661 | 58.6 | 708 | 70.5 | 755 | 20.8 |
| 615 | 34.2 | 662 | 56.7 | 709 | 68.9 | 756 | 19.8 |
| 616 | 33.6 | 663 | 55 | 710 | 67.4 | 757 | 18.9 |
| 617 | 32.1 | 664 | 53.7 | 711 | 66 | 758 | 18 |
| 618 | 30 | 665 | 52.7 | 712 | 64.7 | 759 | 17 |
| 619 | 27.5 | 666 | 51.9 | 713 | 63.7 | 760 | 16.1 |
| 620 | 25.1 | 667 | 51.4 | 714 | 62.9 | 761 | 15.5 |
| 621 | 22.8 | 668 | 51 | 715 | 62.2 | 762 | 14.4 |
| 622 | 20.5 | 669 | 50.7 | 716 | 61.7 | 763 | 14.9 |
| 623 | 17.9 | 670 | 50.6 | 717 | 61.2 | 764 | 15.9 |
| 624 | 15.1 | 671 | 50.8 | 718 | 60.7 | 765 | 17.1 |
| 625 | 13.4 | 672 | 51.2 | 719 | 60.3 | 766 | 18.3 |
| 626 | 12.8 | 673 | 51.7 | 720 | 59.9 | 767 | 19.4 |
| 627 | 13.7 | 674 | 52.3 | 721 | 59.6 | 768 | 20.4 |
| 628 | 16 | 675 | 53.1 | 722 | 59.3 | 769 | 21.2 |
| 629 | 18.1 | 676 | 53.8 | 723 | 59 | 770 | 21.9 |
| 630 | 20.8 | 677 | 54.5 | 724 | 58.6 | 771 | 22.7 |
| 631 | 23.7 | 678 | 55.1 | 725 | 58 | 772 | 23.4 |
| 632 | 26.5 | 679 | 55.9 | 726 | 57.5 | 773 | 24.2 |
| 633 | 29.3 | 680 | 56.5 | 727 | 56.9 | 774 | 24.3 |
| 634 | 32 | 681 | 57.1 | 728 | 56.3 | 775 | 24.2 |
| 635 | 34.5 | 682 | 57.8 | 729 | 55.9 | 776 | 24.1 |
| 636 | 36.8 | 683 | 58.5 | 730 | 55.6 | 777 | 23.8 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 778 | 23 | 827 | 59.9 | 876 | 46.9 | 925 | 49 |
| 779 | 22.6 | 828 | 60.7 | 877 | 47.1 | 926 | 48.5 |
| 780 | 21.7 | 829 | 61.4 | 878 | 47.5 | 927 | 48 |
| 781 | 21.3 | 830 | 62 | 879 | 47.8 | 928 | 47.5 |
| 782 | 20.3 | 831 | 62.5 | 880 | 48.3 | 929 | 47 |
| 783 | 19.1 | 832 | 62.9 | 881 | 48.8 | 930 | 46.9 |
| 784 | 18.1 | 833 | 63.2 | 882 | 49.5 | 931 | 46.8 |
| 785 | 16.9 | 834 | 63.4 | 883 | 50.2 | 932 | 46.8 |
| 786 | 16 | 835 | 63.7 | 884 | 50.8 | 933 | 46.8 |
| 787 | 14.8 | 836 | 64 | 885 | 51.4 | 934 | 46.9 |
| 788 | 14.5 | 837 | 64.4 | 886 | 51.8 | 935 | 46.9 |
| 789 | 13.7 | 838 | 64.9 | 887 | 51.9 | 936 | 46.9 |
| 790 | 13.5 | 839 | 65.5 | 888 | 51.7 | 937 | 46.9 |
| 791 | 12.9 | 840 | 66.2 | 889 | 51.2 | 938 | 46.9 |
| 792 | 12.7 | 841 | 67 | 890 | 50.4 | 939 | 46.8 |
| 793 | 12.5 | 842 | 67.8 | 891 | 49.2 | 940 | 46.6 |
| 794 | 12.5 | 843 | 68.6 | 892 | 47.7 | 941 | 46.4 |
| 795 | 12.6 | 844 | 69.4 | 893 | 46.3 | 942 | 46 |
| 796 | 13 | 845 | 70.1 | 894 | 45.1 | 943 | 45.5 |
| 797 | 13.6 | 846 | 70.9 | 895 | 44.2 | 944 | 45 |
| 798 | 14.6 | 847 | 71.7 | 896 | 43.7 | 945 | 44.5 |
| 799 | 15.7 | 848 | 72.5 | 897 | 43.4 | 946 | 44.2 |
| 800 | 17.1 | 849 | 73.2 | 898 | 43.1 | 947 | 43.9 |
| 801 | 18.7 | 850 | 73.8 | 899 | 42.5 | 948 | 43.7 |
| 802 | 20.2 | 851 | 74.4 | 900 | 41.8 | 949 | 43.6 |
| 803 | 21.9 | 852 | 74.7 | 901 | 41.1 | 950 | 43.6 |
| 804 | 23.6 | 853 | 74.7 | 902 | 40.3 | 951 | 43.5 |
| 805 | 25.4 | 854 | 74.6 | 903 | 39.7 | 952 | 43.5 |
| 806 | 27.1 | 855 | 74.2 | 904 | 39.3 | 953 | 43.4 |
| 807 | 28.9 | 856 | 73.5 | 905 | 39.2 | 954 | 43.3 |
| 808 | 30.4 | 857 | 72.6 | 906 | 39.3 | 955 | 43.1 |
| 809 | 32 | 858 | 71.8 | 907 | 39.6 | 956 | 42.9 |
| 810 | 33.4 | 859 | 71 | 908 | 40 | 957 | 42.7 |
| 811 | 35 | 860 | 70.1 | 909 | 40.7 | 958 | 42.5 |
| 812 | 36.4 | 861 | 69.4 | 910 | 41.4 | 959 | 42.4 |
| 813 | 38.1 | 862 | 68.9 | 911 | 42.2 | 960 | 42.2 |
| 814 | 39.7 | 863 | 68.4 | 912 | 43.1 | 961 | 42.1 |
| 815 | 41.6 | 864 | 67.9 | 913 | 44.1 | 962 | 42 |
| 816 | 43.3 | 865 | 67.1 | 914 | 44.9 | 963 | 41.8 |
| 817 | 45.1 | 866 | 65.8 | 915 | 45.6 | 964 | 41.7 |
| 818 | 46.9 | 867 | 63.9 | 916 | 46.4 | 965 | 41.5 |
| 819 | 48.7 | 868 | 61.4 | 917 | 47 | 966 | 41.3 |
| 820 | 50.5 | 869 | 58.4 | 918 | 47.8 | 967 | 41.1 |
| 821 | 52.4 | 870 | 55.4 | 919 | 48.3 | 968 | 40.8 |
| 822 | 54.1 | 871 | 52.4 | 920 | 48.9 | 969 | 40.3 |
| 823 | 55.7 | 872 | 50 | 921 | 49.4 | 970 | 39.6 |
| 824 | 56.8 | 873 | 48.3 | 922 | 49.8 | 971 | 38.5 |
| 825 | 57.9 | 874 | 47.3 | 923 | 49.6 | 972 | 37 |
| 826 | 59 | 875 | 46.8 | 924 | 49.3 | 973 | 35.1 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 974 | 33 |  |  |  |  |  |  |
| 975 | 30.6 |  |  |  |  |  |  |
| 976 | 27.9 |  |  |  |  |  |  |
| 977 | 25.1 |  |  |  |  |  |  |
| 978 | 22 |  |  |  |  |  |  |
| 979 | 18.8 |  |  |  |  |  |  |
| 980 | 15.5 |  |  |  |  |  |  |
| 981 | 12.3 |  |  |  |  |  |  |
| 982 | 8.8 |  |  |  |  |  |  |
| 983 | 6 |  |  |  |  |  |  |
| 984 | 3.6 |  |  |  |  |  |  |
| 985 | 1.6 |  |  |  |  |  |  |
| 986 | 0 |  |  |  |  |  |  |
| 987 | 0 |  |  |  |  |  |  |
| 988 | 0 |  |  |  |  |  |  |
| 989 | 0 |  |  |  |  |  |  |
| 990 | 0 |  |  |  |  |  |  |
| 991 | 0 |  |  |  |  |  |  |
| 992 | 0 |  |  |  |  |  |  |
| 993 | 0 |  |  |  |  |  |  |
| 994 | 0 |  |  |  |  |  |  |
| 995 | 0 |  |  |  |  |  |  |
| 996 | 0 |  |  |  |  |  |  |
| 997 | 0 |  |  |  |  |  |  |
| 998 | 0 |  |  |  |  |  |  |
| 999 | 0 |  |  |  |  |  |  |
| 1000 | 0 |  |  |  |  |  |  |
| 1001 | 0 |  |  |  |  |  |  |
| 1002 | 0 |  |  |  |  |  |  |
| 1003 | 0 |  |  |  |  |  |  |
| 1004 | 0 |  |  |  |  |  |  |
| 1005 | 0 |  |  |  |  |  |  |
| 1006 | 0 |  |  |  |  |  |  |
| 1007 | 0 |  |  |  |  |  |  |
| 1008 | 0 |  |  |  |  |  |  |
| 1009 | 0 |  |  |  |  |  |  |
| 1010 | 0 |  |  |  |  |  |  |
| 1011 | 0 |  |  |  |  |  |  |
| 1012 | 0 |  |  |  |  |  |  |
| 1013 | 0 |  |  |  |  |  |  |
| 1014 | 0 |  |  |  |  |  |  |
| 1015 | 0 |  |  |  |  |  |  |
| 1016 | 0 |  |  |  |  |  |  |
| 1017 | 0 |  |  |  |  |  |  |
| 1018 | 0 |  |  |  |  |  |  |
| 1019 | 0 |  |  |  |  |  |  |
| 1020 | 0 |  |  |  |  |  |  |
| 1021 | 0 |  |  |  |  |  |  |
| 1022 | 0 |  |  |  |  |  |  |

Table A/5
WLTC, Class 2 vehicles, phase High

| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1023 | 0 | 1070 | 46 | 1117 | 73.9 | 1164 | 71.7 |
| 1024 | 0 | 1071 | 46.4 | 1118 | 74.9 | 1165 | 69.9 |
| 1025 | 0 | 1072 | 47 | 1119 | 75.7 | 1166 | 67.9 |
| 1026 | 0 | 1073 | 47.4 | 1120 | 76.4 | 1167 | 65.7 |
| 1027 | 1.1 | 1074 | 48 | 1121 | 77.1 | 1168 | 63.5 |
| 1028 | 3 | 1075 | 48.4 | 1122 | 77.6 | 1169 | 61.2 |
| 1029 | 5.7 | 1076 | 49 | 1123 | 78 | 1170 | 59 |
| 1030 | 8.4 | 1077 | 49.4 | 1124 | 78.2 | 1171 | 56.8 |
| 1031 | 11.1 | 1078 | 50 | 1125 | 78.4 | 1172 | 54.7 |
| 1032 | 14 | 1079 | 50.4 | 1126 | 78.5 | 1173 | 52.7 |
| 1033 | 17 | 1080 | 50.8 | 1127 | 78.5 | 1174 | 50.9 |
| 1034 | 20.1 | 1081 | 51.1 | 1128 | 78.6 | 1175 | 49.4 |
| 1035 | 22.7 | 1082 | 51.3 | 1129 | 78.7 | 1176 | 48.1 |
| 1036 | 23.6 | 1083 | 51.3 | 1130 | 78.9 | 1177 | 47.1 |
| 1037 | 24.5 | 1084 | 51.3 | 1131 | 79.1 | 1178 | 46.5 |
| 1038 | 24.8 | 1085 | 51.3 | 1132 | 79.4 | 1179 | 46.3 |
| 1039 | 25.1 | 1086 | 51.3 | 1133 | 79.8 | 1180 | 46.5 |
| 1040 | 25.3 | 1087 | 51.3 | 1134 | 80.1 | 1181 | 47.2 |
| 1041 | 25.5 | 1088 | 51.3 | 1135 | 80.5 | 1182 | 48.3 |
| 1042 | 25.7 | 1089 | 51.4 | 1136 | 80.8 | 1183 | 49.7 |
| 1043 | 25.8 | 1090 | 51.6 | 1137 | 81 | 1184 | 51.3 |
| 1044 | 25.9 | 1091 | 51.8 | 1138 | 81.2 | 1185 | 53 |
| 1045 | 26 | 1092 | 52.1 | 1139 | 81.3 | 1186 | 54.9 |
| 1046 | 26.1 | 1093 | 52.3 | 1140 | 81.2 | 1187 | 56.7 |
| 1047 | 26.3 | 1094 | 52.6 | 1141 | 81 | 1188 | 58.6 |
| 1048 | 26.5 | 1095 | 52.8 | 1142 | 80.6 | 1189 | 60.2 |
| 1049 | 26.8 | 1096 | 52.9 | 1143 | 80 | 1190 | 61.6 |
| 1050 | 27.1 | 1097 | 53 | 1144 | 79.1 | 1191 | 62.2 |
| 1051 | 27.5 | 1098 | 53 | 1145 | 78 | 1192 | 62.5 |
| 1052 | 28 | 1099 | 53 | 1146 | 76.8 | 1193 | 62.8 |
| 1053 | 28.6 | 1100 | 53.1 | 1147 | 75.5 | 1194 | 62.9 |
| 1054 | 29.3 | 1101 | 53.2 | 1148 | 74.1 | 1195 | 63 |
| 1055 | 30.4 | 1102 | 53.3 | 1149 | 72.9 | 1196 | 63 |
| 1056 | 31.8 | 1103 | 53.4 | 1150 | 71.9 | 1197 | 63.1 |
| 1057 | 33.7 | 1104 | 53.5 | 1151 | 71.2 | 1198 | 63.2 |
| 1058 | 35.8 | 1105 | 53.7 | 1152 | 70.9 | 1199 | 63.3 |
| 1059 | 37.8 | 1106 | 55 | 1153 | 71 | 1200 | 63.5 |
| 1060 | 39.5 | 1107 | 56.8 | 1154 | 71.5 | 1201 | 63.7 |
| 1061 | 40.8 | 1108 | 58.8 | 1155 | 72.3 | 1202 | 63.9 |
| 1062 | 41.8 | 1109 | 60.9 | 1156 | 73.2 | 1203 | 64.1 |
| 1063 | 42.4 | 1110 | 63 | 1157 | 74.1 | 1204 | 64.3 |
| 1064 | 43 | 1111 | 65 | 1158 | 74.9 | 1205 | 66.1 |
| 1065 | 43.4 | 1112 | 66.9 | 1159 | 75.4 | 1206 | 67.9 |
| 1066 | 44 | 1113 | 68.6 | 1160 | 75.5 | 1207 | 69.7 |
| 1067 | 44.4 | 1114 | 70.1 | 1161 | 75.2 | 1208 | 71.4 |
| 1068 | 45 | 1115 | 71.5 | 1162 | 74.5 | 1209 | 73.1 |
| 1069 | 45.4 | 1116 | 72.8 | 1163 | 73.3 | 1210 | 74.7 |


| Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1211 | 76.2 | 1260 | 35.4 | 1309 | 72.3 | 1358 | 70.8 |
| 1212 | 77.5 | 1261 | 32.7 | 1310 | 71.9 | 1359 | 70.8 |
| 1213 | 78.6 | 1262 | 30 | 1311 | 71.3 | 1360 | 70.9 |
| 1214 | 79.7 | 1263 | 29.9 | 1312 | 70.9 | 1361 | 70.9 |
| 1215 | 80.6 | 1264 | 30 | 1313 | 70.5 | 1362 | 70.9 |
| 1216 | 81.5 | 1265 | 30.2 | 1314 | 70 | 1363 | 70.9 |
| 1217 | 82.2 | 1266 | 30.4 | 1315 | 69.6 | 1364 | 71 |
| 1218 | 83 | 1267 | 30.6 | 1316 | 69.2 | 1365 | 71 |
| 1219 | 83.7 | 1268 | 31.6 | 1317 | 68.8 | 1366 | 71.1 |
| 1220 | 84.4 | 1269 | 33 | 1318 | 68.4 | 1367 | 71.2 |
| 1221 | 84.9 | 1270 | 33.9 | 1319 | 67.9 | 1368 | 71.3 |
| 1222 | 85.1 | 1271 | 34.8 | 1320 | 67.5 | 1369 | 71.4 |
| 1223 | 85.2 | 1272 | 35.7 | 1321 | 67.2 | 1370 | 71.5 |
| 1224 | 84.9 | 1273 | 36.6 | 1322 | 66.8 | 1371 | 71.7 |
| 1225 | 84.4 | 1274 | 37.5 | 1323 | 65.6 | 1372 | 71.8 |
| 1226 | 83.6 | 1275 | 38.4 | 1324 | 63.3 | 1373 | 71.9 |
| 1227 | 82.7 | 1276 | 39.3 | 1325 | 60.2 | 1374 | 71.9 |
| 1228 | 81.5 | 1277 | 40.2 | 1326 | 56.2 | 1375 | 71.9 |
| 1229 | 80.1 | 1278 | 40.8 | 1327 | 52.2 | 1376 | 71.9 |
| 1230 | 78.7 | 1279 | 41.7 | 1328 | 48.4 | 1377 | 71.9 |
| 1231 | 77.4 | 1280 | 42.4 | 1329 | 45 | 1378 | 71.9 |
| 1232 | 76.2 | 1281 | 43.1 | 1330 | 41.6 | 1379 | 71.9 |
| 1233 | 75.4 | 1282 | 43.6 | 1331 | 38.6 | 1380 | 72 |
| 1234 | 74.8 | 1283 | 44.2 | 1332 | 36.4 | 1381 | 72.1 |
| 1235 | 74.3 | 1284 | 44.8 | 1333 | 34.8 | 1382 | 72.4 |
| 1236 | 73.8 | 1285 | 45.5 | 1334 | 34.2 | 1383 | 72.7 |
| 1237 | 73.2 | 1286 | 46.3 | 1335 | 34.7 | 1384 | 73.1 |
| 1238 | 72.4 | 1287 | 47.2 | 1336 | 36.3 | 1385 | 73.4 |
| 1239 | 71.6 | 1288 | 48.1 | 1337 | 38.5 | 1386 | 73.8 |
| 1240 | 70.8 | 1289 | 49.1 | 1338 | 41 | 1387 | 74 |
| 1241 | 69.9 | 1290 | 50 | 1339 | 43.7 | 1388 | 74.1 |
| 1242 | 67.9 | 1291 | 51 | 1340 | 46.5 | 1389 | 74 |
| 1243 | 65.7 | 1292 | 51.9 | 1341 | 49.1 | 1390 | 73 |
| 1244 | 63.5 | 1293 | 52.7 | 1342 | 51.6 | 1391 | 72 |
| 1245 | 61.2 | 1294 | 53.7 | 1343 | 53.9 | 1392 | 71 |
| 1246 | 59 | 1295 | 55 | 1344 | 56 | 1393 | 70 |
| 1247 | 56.8 | 1296 | 56.8 | 1345 | 57.9 | 1394 | 69 |
| 1248 | 54.7 | 1297 | 58.8 | 1346 | 59.7 | 1395 | 68 |
| 1249 | 52.7 | 1298 | 60.9 | 1347 | 61.2 | 1396 | 67.7 |
| 1250 | 50.9 | 1299 | 63 | 1348 | 62.5 | 1397 | 66.7 |
| 1251 | 49.4 | 1300 | 65 | 1349 | 63.5 | 1398 | 66.6 |
| 1252 | 48.1 | 1301 | 66.9 | 1350 | 64.3 | 1399 | 66.7 |
| 1253 | 47.1 | 1302 | 68.6 | 1351 | 65.3 | 1400 | 66.8 |
| 1254 | 46.5 | 1303 | 70.1 | 1352 | 66.3 | 1401 | 66.9 |
| 1255 | 46.3 | 1304 | 71 | 1353 | 67.3 | 1402 | 66.9 |
| 1256 | 45.1 | 1305 | 71.8 | 1354 | 68.3 | 1403 | 66.9 |
| 1257 | 43 | 1306 | 72.8 | 1355 | 69.3 | 1404 | 66.9 |
| 1258 | 40.6 | 1307 | 72.9 | 1356 | 70.3 | 1405 | 66.9 |
| 1259 | 38.1 | 1308 | 73 | 1357 | 70.8 | 1406 | 66.9 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1407 | 66.9 | 1456 | 0 |  |  |  |  |
| 1408 | 67 | 1457 | 0 |  |  |  |  |
| 1409 | 67.1 | 1458 | 0 |  |  |  |  |
| 1410 | 67.3 | 1459 | 0 |  |  |  |  |
| 1411 | 67.5 | 1460 | 0 |  |  |  |  |
| 1412 | 67.8 | 1461 | 0 |  |  |  |  |
| 1413 | 68.2 | 1462 | 0 |  |  |  |  |
| 1414 | 68.6 | 1463 | 0 |  |  |  |  |
| 1415 | 69 | 1464 | 0 |  |  |  |  |
| 1416 | 69.3 | 1465 | 0 |  |  |  |  |
| 1417 | 69.3 | 1466 | 0 |  |  |  |  |
| 1418 | 69.2 | 1467 | 0 |  |  |  |  |
| 1419 | 68.8 | 1468 | 0 |  |  |  |  |
| 1420 | 68.2 | 1469 | 0 |  |  |  |  |
| 1421 | 67.6 | 1470 | 0 |  |  |  |  |
| 1422 | 67.4 | 1471 | 0 |  |  |  |  |
| 1423 | 67.2 | 1472 | 0 |  |  |  |  |
| 1424 | 66.9 | 1473 | 0 |  |  |  |  |
| 1425 | 66.3 | 1474 | 0 |  |  |  |  |
| 1426 | 65.4 | 1475 | 0 |  |  |  |  |
| 1427 | 64 | 1476 | 0 |  |  |  |  |
| 1428 | 62.4 | 1477 | 0 |  |  |  |  |
| 1429 | 60.6 |  |  |  |  |  |  |
| 1430 | 58.6 |  |  |  |  |  |  |
| 1431 | 56.7 |  |  |  |  |  |  |
| 1432 | 54.8 |  |  |  |  |  |  |
| 1433 | 53 |  |  |  |  |  |  |
| 1434 | 51.3 |  |  |  |  |  |  |
| 1435 | 49.6 |  |  |  |  |  |  |
| 1436 | 47.8 |  |  |  |  |  |  |
| 1437 | 45.5 |  |  |  |  |  |  |
| 1438 | 42.8 |  |  |  |  |  |  |
| 1439 | 39.8 |  |  |  |  |  |  |
| 1440 | 36.5 |  |  |  |  |  |  |
| 1441 | 33 |  |  |  |  |  |  |
| 1442 | 29.5 |  |  |  |  |  |  |
| 1443 | 25.8 |  |  |  |  |  |  |
| 1444 | 22.1 |  |  |  |  |  |  |
| 1445 | 18.6 |  |  |  |  |  |  |
| 1446 | 15.3 |  |  |  |  |  |  |
| 1447 | 12.4 |  |  |  |  |  |  |
| 1448 | 9.6 |  |  |  |  |  |  |
| 1449 | 6.6 |  |  |  |  |  |  |
| 1450 | 3.8 |  |  |  |  |  |  |
| 1451 | 1.6 |  |  |  |  |  |  |
| 1452 | 0 |  |  |  |  |  |  |
| 1453 | 0 |  |  |  |  |  |  |
| 1454 | 0 |  |  |  |  |  |  |
| 1455 | 0 |  |  |  |  |  |  |

Table A/6
WLTC, Class 2 vehicles, phase Extra High

| Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1478 | 0 | 1525 | 63.4 | 1572 | 107.4 | 1619 | 113.7 |
| 1479 | 1.1 | 1526 | 64.5 | 1573 | 108.7 | 1620 | 114.1 |
| 1480 | 2.3 | 1527 | 65.7 | 1574 | 109.9 | 1621 | 114.4 |
| 1481 | 4.6 | 1528 | 66.9 | 1575 | 111.2 | 1622 | 114.6 |
| 1482 | 6.5 | 1529 | 68.1 | 1576 | 112.3 | 1623 | 114.7 |
| 1483 | 8.9 | 1530 | 69.1 | 1577 | 113.4 | 1624 | 114.7 |
| 1484 | 10.9 | 1531 | 70 | 1578 | 114.4 | 1625 | 114.7 |
| 1485 | 13.5 | 1532 | 70.9 | 1579 | 115.3 | 1626 | 114.6 |
| 1486 | 15.2 | 1533 | 71.8 | 1580 | 116.1 | 1627 | 114.5 |
| 1487 | 17.6 | 1534 | 72.6 | 1581 | 116.8 | 1628 | 114.5 |
| 1488 | 19.3 | 1535 | 73.4 | 1582 | 117.4 | 1629 | 114.5 |
| 1489 | 21.4 | 1536 | 74 | 1583 | 117.7 | 1630 | 114.7 |
| 1490 | 23 | 1537 | 74.7 | 1584 | 118.2 | 1631 | 115 |
| 1491 | 25 | 1538 | 75.2 | 1585 | 118.1 | 1632 | 115.6 |
| 1492 | 26.5 | 1539 | 75.7 | 1586 | 117.7 | 1633 | 116.4 |
| 1493 | 28.4 | 1540 | 76.4 | 1587 | 117 | 1634 | 117.3 |
| 1494 | 29.8 | 1541 | 77.2 | 1588 | 116.1 | 1635 | 118.2 |
| 1495 | 31.7 | 1542 | 78.2 | 1589 | 115.2 | 1636 | 118.8 |
| 1496 | 33.7 | 1543 | 78.9 | 1590 | 114.4 | 1637 | 119.3 |
| 1497 | 35.8 | 1544 | 79.9 | 1591 | 113.6 | 1638 | 119.6 |
| 1498 | 38.1 | 1545 | 81.1 | 1592 | 113 | 1639 | 119.7 |
| 1499 | 40.5 | 1546 | 82.4 | 1593 | 112.6 | 1640 | 119.5 |
| 1500 | 42.2 | 1547 | 83.7 | 1594 | 112.2 | 1641 | 119.3 |
| 1501 | 43.5 | 1548 | 85.4 | 1595 | 111.9 | 1642 | 119.2 |
| 1502 | 44.5 | 1549 | 87 | 1596 | 111.6 | 1643 | 119 |
| 1503 | 45.2 | 1550 | 88.3 | 1597 | 111.2 | 1644 | 118.8 |
| 1504 | 45.8 | 1551 | 89.5 | 1598 | 110.7 | 1645 | 118.8 |
| 1505 | 46.6 | 1552 | 90.5 | 1599 | 110.1 | 1646 | 118.8 |
| 1506 | 47.4 | 1553 | 91.3 | 1600 | 109.3 | 1647 | 118.8 |
| 1507 | 48.5 | 1554 | 92.2 | 1601 | 108.4 | 1648 | 118.8 |
| 1508 | 49.7 | 1555 | 93 | 1602 | 107.4 | 1649 | 118.9 |
| 1509 | 51.3 | 1556 | 93.8 | 1603 | 106.7 | 1650 | 119 |
| 1510 | 52.9 | 1557 | 94.6 | 1604 | 106.3 | 1651 | 119 |
| 1511 | 54.3 | 1558 | 95.3 | 1605 | 106.2 | 1652 | 119.1 |
| 1512 | 55.6 | 1559 | 95.9 | 1606 | 106.4 | 1653 | 119.2 |
| 1513 | 56.8 | 1560 | 96.6 | 1607 | 107 | 1654 | 119.4 |
| 1514 | 57.9 | 1561 | 97.4 | 1608 | 107.5 | 1655 | 119.6 |
| 1515 | 58.9 | 1562 | 98.1 | 1609 | 107.9 | 1656 | 119.9 |
| 1516 | 59.7 | 1563 | 98.7 | 1610 | 108.4 | 1657 | 120.1 |
| 1517 | 60.3 | 1564 | 99.5 | 1611 | 108.9 | 1658 | 120.3 |
| 1518 | 60.7 | 1565 | 100.3 | 1612 | 109.5 | 1659 | 120.4 |
| 1519 | 60.9 | 1566 | 101.1 | 1613 | 110.2 | 1660 | 120.5 |
| 1520 | 61 | 1567 | 101.9 | 1614 | 110.9 | 1661 | 120.5 |
| 1521 | 61.1 | 1568 | 102.8 | 1615 | 111.6 | 1662 | 120.5 |
| 1522 | 61.4 | 1569 | 103.8 | 1616 | 112.2 | 1663 | 120.5 |
| 1523 | 61.8 | 1570 | 105 | 1617 | 112.8 | 1664 | 120.4 |
| 1524 | 62.5 | 1571 | 106.1 | 1618 | 113.3 | 1665 | 120.3 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1666 | 120.1 | 1715 | 120.4 | 1764 | 82.6 |  |  |
| 1667 | 119.9 | 1716 | 120.8 | 1765 | 81.9 |  |  |
| 1668 | 119.6 | 1717 | 121.1 | 1766 | 81.1 |  |  |
| 1669 | 119.5 | 1718 | 121.6 | 1767 | 80 |  |  |
| 1670 | 119.4 | 1719 | 121.8 | 1768 | 78.7 |  |  |
| 1671 | 119.3 | 1720 | 122.1 | 1769 | 76.9 |  |  |
| 1672 | 119.3 | 1721 | 122.4 | 1770 | 74.6 |  |  |
| 1673 | 119.4 | 1722 | 122.7 | 1771 | 72 |  |  |
| 1674 | 119.5 | 1723 | 122.8 | 1772 | 69 |  |  |
| 1675 | 119.5 | 1724 | 123.1 | 1773 | 65.6 |  |  |
| 1676 | 119.6 | 1725 | 123.1 | 1774 | 62.1 |  |  |
| 1677 | 119.6 | 1726 | 122.8 | 1775 | 58.5 |  |  |
| 1678 | 119.6 | 1727 | 122.3 | 1776 | 54.7 |  |  |
| 1679 | 119.4 | 1728 | 121.3 | 1777 | 50.9 |  |  |
| 1680 | 119.3 | 1729 | 119.9 | 1778 | 47.3 |  |  |
| 1681 | 119 | 1730 | 118.1 | 1779 | 43.8 |  |  |
| 1682 | 118.8 | 1731 | 115.9 | 1780 | 40.4 |  |  |
| 1683 | 118.7 | 1732 | 113.5 | 1781 | 37.4 |  |  |
| 1684 | 118.8 | 1733 | 111.1 | 1782 | 34.3 |  |  |
| 1685 | 119 | 1734 | 108.6 | 1783 | 31.3 |  |  |
| 1686 | 119.2 | 1735 | 106.2 | 1784 | 28.3 |  |  |
| 1687 | 119.6 | 1736 | 104 | 1785 | 25.2 |  |  |
| 1688 | 120 | 1737 | 101.1 | 1786 | 22 |  |  |
| 1689 | 120.3 | 1738 | 98.3 | 1787 | 18.9 |  |  |
| 1690 | 120.5 | 1739 | 95.7 | 1788 | 16.1 |  |  |
| 1691 | 120.7 | 1740 | 93.5 | 1789 | 13.4 |  |  |
| 1692 | 120.9 | 1741 | 91.5 | 1790 | 11.1 |  |  |
| 1693 | 121 | 1742 | 90.7 | 1791 | 8.9 |  |  |
| 1694 | 121.1 | 1743 | 90.4 | 1792 | 6.9 |  |  |
| 1695 | 121.2 | 1744 | 90.2 | 1793 | 4.9 |  |  |
| 1696 | 121.3 | 1745 | 90.2 | 1794 | 2.8 |  |  |
| 1697 | 121.4 | 1746 | 90.1 | 1795 | 0 |  |  |
| 1698 | 121.5 | 1747 | 90 | 1796 | 0 |  |  |
| 1699 | 121.5 | 1748 | 89.8 | 1797 | 0 |  |  |
| 1700 | 121.5 | 1749 | 89.6 | 1798 | 0 |  |  |
| 1701 | 121.4 | 1750 | 89.4 | 1799 | 0 |  |  |
| 1702 | 121.3 | 1751 | 89.2 | 1800 | 0 |  |  |
| 1703 | 121.1 | 1752 | 88.9 |  |  |  |  |
| 1704 | 120.9 | 1753 | 88.5 |  |  |  |  |
| 1705 | 120.6 | 1754 | 88.1 |  |  |  |  |
| 1706 | 120.4 | 1755 | 87.6 |  |  |  |  |
| 1707 | 120.2 | 1756 | 87.1 |  |  |  |  |
| 1708 | 120.1 | 1757 | 86.6 |  |  |  |  |
| 1709 | 119.9 | 1758 | 86.1 |  |  |  |  |
| 1710 | 119.8 | 1759 | 85.5 |  |  |  |  |
| 1711 | 119.8 | 1760 | 85 |  |  |  |  |
| 1712 | 119.9 | 1761 | 84.4 |  |  |  |  |
| 1713 | 120 | 1762 | 83.8 |  |  |  |  |
| 1714 | 120.2 | 1763 | 83.2 |  |  |  |  |

Table A/7
WLTC, Class 3 vehicles, phase Low

| Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 47 | 19.5 | 94 | 12 | 141 | 11.7 |
| 1 | 0 | 48 | 18.4 | 95 | 9.1 | 142 | 16.4 |
| 2 | 0 | 49 | 17.8 | 96 | 5.8 | 143 | 18.9 |
| 3 | 0 | 50 | 17.8 | 97 | 3.6 | 144 | 19.9 |
| 4 | 0 | 51 | 17.4 | 98 | 2.2 | 145 | 20.8 |
| 5 | 0 | 52 | 15.7 | 99 | 0 | 146 | 22.8 |
| 6 | 0 | 53 | 13.1 | 100 | 0 | 147 | 25.4 |
| 7 | 0 | 54 | 12.1 | 101 | 0 | 148 | 27.7 |
| 8 | 0 | 55 | 12 | 102 | 0 | 149 | 29.2 |
| 9 | 0 | 56 | 12 | 103 | 0 | 150 | 29.8 |
| 10 | 0 | 57 | 12 | 104 | 0 | 151 | 29.4 |
| 11 | 0 | 58 | 12.3 | 105 | 0 | 152 | 27.2 |
| 12 | 0.2 | 59 | 12.6 | 106 | 0 | 153 | 22.6 |
| 13 | 1.7 | 60 | 14.7 | 107 | 0 | 154 | 17.3 |
| 14 | 5.4 | 61 | 15.3 | 108 | 0 | 155 | 13.3 |
| 15 | 9.9 | 62 | 15.9 | 109 | 0 | 156 | 12 |
| 16 | 13.1 | 63 | 16.2 | 110 | 0 | 157 | 12.6 |
| 17 | 16.9 | 64 | 17.1 | 111 | 0 | 158 | 14.1 |
| 18 | 21.7 | 65 | 17.8 | 112 | 0 | 159 | 17.2 |
| 19 | 26 | 66 | 18.1 | 113 | 0 | 160 | 20.1 |
| 20 | 27.5 | 67 | 18.4 | 114 | 0 | 161 | 23.4 |
| 21 | 28.1 | 68 | 20.3 | 115 | 0 | 162 | 25.5 |
| 22 | 28.3 | 69 | 23.2 | 116 | 0 | 163 | 27.6 |
| 23 | 28.8 | 70 | 26.5 | 117 | 0 | 164 | 29.5 |
| 24 | 29.1 | 71 | 29.8 | 118 | 0 | 165 | 31.1 |
| 25 | 30.8 | 72 | 32.6 | 119 | 0 | 166 | 32.1 |
| 26 | 31.9 | 73 | 34.4 | 120 | 0 | 167 | 33.2 |
| 27 | 34.1 | 74 | 35.5 | 121 | 0 | 168 | 35.2 |
| 28 | 36.6 | 75 | 36.4 | 122 | 0 | 169 | 37.2 |
| 29 | 39.1 | 76 | 37.4 | 123 | 0 | 170 | 38 |
| 30 | 41.3 | 77 | 38.5 | 124 | 0 | 171 | 37.4 |
| 31 | 42.5 | 78 | 39.3 | 125 | 0 | 172 | 35.1 |
| 32 | 43.3 | 79 | 39.5 | 126 | 0 | 173 | 31 |
| 33 | 43.9 | 80 | 39 | 127 | 0 | 174 | 27.1 |
| 34 | 44.4 | 81 | 38.5 | 128 | 0 | 175 | 25.3 |
| 35 | 44.5 | 82 | 37.3 | 129 | 0 | 176 | 25.1 |
| 36 | 44.2 | 83 | 37 | 130 | 0 | 177 | 25.9 |
| 37 | 42.7 | 84 | 36.7 | 131 | 0 | 178 | 27.8 |
| 38 | 39.9 | 85 | 35.9 | 132 | 0 | 179 | 29.2 |
| 39 | 37 | 86 | 35.3 | 133 | 0 | 180 | 29.6 |
| 40 | 34.6 | 87 | 34.6 | 134 | 0 | 181 | 29.5 |
| 41 | 32.3 | 88 | 34.2 | 135 | 0 | 182 | 29.2 |
| 42 | 29 | 89 | 31.9 | 136 | 0 | 183 | 28.3 |
| 43 | 25.1 | 90 | 27.3 | 137 | 0 | 184 | 26.1 |
| 44 | 22.2 | 91 | 22 | 138 | 0.2 | 185 | 23.6 |
| 45 | 20.9 | 92 | 17 | 139 | 1.9 | 186 | 21 |
| 46 | 20.4 | 93 | 14.2 | 140 | 6.1 | 187 | 18.9 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 188 | 17.1 | 237 | 49.2 | 286 | 37.4 | 335 | 15 |
| 189 | 15.7 | 238 | 48.4 | 287 | 40.7 | 336 | 14.5 |
| 190 | 14.5 | 239 | 46.9 | 288 | 44 | 337 | 14.3 |
| 191 | 13.7 | 240 | 44.3 | 289 | 47.3 | 338 | 14.5 |
| 192 | 12.9 | 241 | 41.5 | 290 | 49.2 | 339 | 15.4 |
| 193 | 12.5 | 242 | 39.5 | 291 | 49.8 | 340 | 17.8 |
| 194 | 12.2 | 243 | 37 | 292 | 49.2 | 341 | 21.1 |
| 195 | 12 | 244 | 34.6 | 293 | 48.1 | 342 | 24.1 |
| 196 | 12 | 245 | 32.3 | 294 | 47.3 | 343 | 25 |
| 197 | 12 | 246 | 29 | 295 | 46.8 | 344 | 25.3 |
| 198 | 12 | 247 | 25.1 | 296 | 46.7 | 345 | 25.5 |
| 199 | 12.5 | 248 | 22.2 | 297 | 46.8 | 346 | 26.4 |
| 200 | 13 | 249 | 20.9 | 298 | 47.1 | 347 | 26.6 |
| 201 | 14 | 250 | 20.4 | 299 | 47.3 | 348 | 27.1 |
| 202 | 15 | 251 | 19.5 | 300 | 47.3 | 349 | 27.7 |
| 203 | 16.5 | 252 | 18.4 | 301 | 47.1 | 350 | 28.1 |
| 204 | 19 | 253 | 17.8 | 302 | 46.6 | 351 | 28.2 |
| 205 | 21.2 | 254 | 17.8 | 303 | 45.8 | 352 | 28.1 |
| 206 | 23.8 | 255 | 17.4 | 304 | 44.8 | 353 | 28 |
| 207 | 26.9 | 256 | 15.7 | 305 | 43.3 | 354 | 27.9 |
| 208 | 29.6 | 257 | 14.5 | 306 | 41.8 | 355 | 27.9 |
| 209 | 32 | 258 | 15.4 | 307 | 40.8 | 356 | 28.1 |
| 210 | 35.2 | 259 | 17.9 | 308 | 40.3 | 357 | 28.2 |
| 211 | 37.5 | 260 | 20.6 | 309 | 40.1 | 358 | 28 |
| 212 | 39.2 | 261 | 23.2 | 310 | 39.7 | 359 | 26.9 |
| 213 | 40.5 | 262 | 25.7 | 311 | 39.2 | 360 | 25 |
| 214 | 41.6 | 263 | 28.7 | 312 | 38.5 | 361 | 23.2 |
| 215 | 43.1 | 264 | 32.5 | 313 | 37.4 | 362 | 21.9 |
| 216 | 45 | 265 | 36.1 | 314 | 36 | 363 | 21.1 |
| 217 | 47.1 | 266 | 39 | 315 | 34.4 | 364 | 20.7 |
| 218 | 49 | 267 | 40.8 | 316 | 33 | 365 | 20.7 |
| 219 | 50.6 | 268 | 42.9 | 317 | 31.7 | 366 | 20.8 |
| 220 | 51.8 | 269 | 44.4 | 318 | 30 | 367 | 21.2 |
| 221 | 52.7 | 270 | 45.9 | 319 | 28 | 368 | 22.1 |
| 222 | 53.1 | 271 | 46 | 320 | 26.1 | 369 | 23.5 |
| 223 | 53.5 | 272 | 45.6 | 321 | 25.6 | 370 | 24.3 |
| 224 | 53.8 | 273 | 45.3 | 322 | 24.9 | 371 | 24.5 |
| 225 | 54.2 | 274 | 43.7 | 323 | 24.9 | 372 | 23.8 |
| 226 | 54.8 | 275 | 40.8 | 324 | 24.3 | 373 | 21.3 |
| 227 | 55.3 | 276 | 38 | 325 | 23.9 | 374 | 17.7 |
| 228 | 55.8 | 277 | 34.4 | 326 | 23.9 | 375 | 14.4 |
| 229 | 56.2 | 278 | 30.9 | 327 | 23.6 | 376 | 11.9 |
| 230 | 56.5 | 279 | 25.5 | 328 | 23.3 | 377 | 10.2 |
| 231 | 56.5 | 280 | 21.4 | 329 | 20.5 | 378 | 8.9 |
| 232 | 56.2 | 281 | 20.2 | 330 | 17.5 | 379 | 8 |
| 233 | 54.9 | 282 | 22.9 | 331 | 16.9 | 380 | 7.2 |
| 234 | 52.9 | 283 | 26.6 | 332 | 16.7 | 381 | 6.1 |
| 235 | 51 | 284 | 30.2 | 333 | 15.9 | 382 | 4.9 |
| 236 | 49.8 | 285 | 34.1 | 334 | 15.6 | 383 | 3.7 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 384 | 2.3 | 433 | 31.3 | 482 | 0 | 531 | 0 |
| 385 | 0.9 | 434 | 31.1 | 483 | 0 | 532 | 0 |
| 386 | 0 | 435 | 30.6 | 484 | 0 | 533 | 0.2 |
| 387 | 0 | 436 | 29.2 | 485 | 0 | 534 | 1.2 |
| 388 | 0 | 437 | 26.7 | 486 | 0 | 535 | 3.2 |
| 389 | 0 | 438 | 23 | 487 | 0 | 536 | 5.2 |
| 390 | 0 | 439 | 18.2 | 488 | 0 | 537 | 8.2 |
| 391 | 0 | 440 | 12.9 | 489 | 0 | 538 | 13 |
| 392 | 0.5 | 441 | 7.7 | 490 | 0 | 539 | 18.8 |
| 393 | 2.1 | 442 | 3.8 | 491 | 0 | 540 | 23.1 |
| 394 | 4.8 | 443 | 1.3 | 492 | 0 | 541 | 24.5 |
| 395 | 8.3 | 444 | 0.2 | 493 | 0 | 542 | 24.5 |
| 396 | 12.3 | 445 | 0 | 494 | 0 | 543 | 24.3 |
| 397 | 16.6 | 446 | 0 | 495 | 0 | 544 | 23.6 |
| 398 | 20.9 | 447 | 0 | 496 | 0 | 545 | 22.3 |
| 399 | 24.2 | 448 | 0 | 497 | 0 | 546 | 20.1 |
| 400 | 25.6 | 449 | 0 | 498 | 0 | 547 | 18.5 |
| 401 | 25.6 | 450 | 0 | 499 | 0 | 548 | 17.2 |
| 402 | 24.9 | 451 | 0 | 500 | 0 | 549 | 16.3 |
| 403 | 23.3 | 452 | 0 | 501 | 0 | 550 | 15.4 |
| 404 | 21.6 | 453 | 0 | 502 | 0 | 551 | 14.7 |
| 405 | 20.2 | 454 | 0 | 503 | 0 | 552 | 14.3 |
| 406 | 18.7 | 455 | 0 | 504 | 0 | 553 | 13.7 |
| 407 | 17 | 456 | 0 | 505 | 0 | 554 | 13.3 |
| 408 | 15.3 | 457 | 0 | 506 | 0 | 555 | 13.1 |
| 409 | 14.2 | 458 | 0 | 507 | 0 | 556 | 13.1 |
| 410 | 13.9 | 459 | 0 | 508 | 0 | 557 | 13.3 |
| 411 | 14 | 460 | 0 | 509 | 0 | 558 | 13.8 |
| 412 | 14.2 | 461 | 0 | 510 | 0 | 559 | 14.5 |
| 413 | 14.5 | 462 | 0 | 511 | 0 | 560 | 16.5 |
| 414 | 14.9 | 463 | 0 | 512 | 0.5 | 561 | 17 |
| 415 | 15.9 | 464 | 0 | 513 | 2.5 | 562 | 17 |
| 416 | 17.4 | 465 | 0 | 514 | 6.6 | 563 | 17 |
| 417 | 18.7 | 466 | 0 | 515 | 11.8 | 564 | 15.4 |
| 418 | 19.1 | 467 | 0 | 516 | 16.8 | 565 | 10.1 |
| 419 | 18.8 | 468 | 0 | 517 | 20.5 | 566 | 4.8 |
| 420 | 17.6 | 469 | 0 | 518 | 21.9 | 567 | 0 |
| 421 | 16.6 | 470 | 0 | 519 | 21.9 | 568 | 0 |
| 422 | 16.2 | 471 | 0 | 520 | 21.3 | 569 | 0 |
| 423 | 16.4 | 472 | 0 | 521 | 20.3 | 570 | 0 |
| 424 | 17.2 | 473 | 0 | 522 | 19.2 | 571 | 0 |
| 425 | 19.1 | 474 | 0 | 523 | 17.8 | 572 | 0 |
| 426 | 22.6 | 475 | 0 | 524 | 15.5 | 573 | 0 |
| 427 | 27.4 | 476 | 0 | 525 | 11.9 | 574 | 0 |
| 428 | 31.6 | 477 | 0 | 526 | 7.6 | 575 | 0 |
| 429 | 33.4 | 478 | 0 | 527 | 4 | 576 | 0 |
| 430 | 33.5 | 479 | 0 | 528 | 2 | 577 | 0 |
| 431 | 32.8 | 480 | 0 | 529 | 1 | 578 | 0 |
| 432 | 31.9 | 481 | 0 | 530 | 0 | 579 | 0 |

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| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| speed in $\mathrm{km} / \mathrm{h}$ |  |  |  |  |  |  |
| 580 | 0 |  |  |  |  |  |
| 581 | 0 |  |  |  |  |  |
| 582 | 0 |  |  |  |  |  |
| 583 | 0 |  |  |  |  |  |
| 584 | 0 |  |  |  |  |  |
| 585 | 0 |  |  |  |  |  |
| 586 | 0 |  |  |  |  |  |
| 587 | 0 |  |  |  |  |  |
| 588 | 0 |  |  |  |  |  |
| 589 | 0 |  |  |  |  |  |

Table A/8
WLTC, Class 3 vehicles of which maximum speed is less than $120 \mathrm{~km} / \mathrm{h}$, phase Medium

| Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 590 | 0 | 637 | 53 | 684 | 18.9 | 731 | 41.9 |
| 591 | 0 | 638 | 53 | 685 | 18.9 | 732 | 42 |
| 592 | 0 | 639 | 52.9 | 686 | 21.3 | 733 | 42.2 |
| 593 | 0 | 640 | 52.7 | 687 | 23.9 | 734 | 42.4 |
| 594 | 0 | 641 | 52.6 | 688 | 25.9 | 735 | 42.7 |
| 595 | 0 | 642 | 53.1 | 689 | 28.4 | 736 | 43.1 |
| 596 | 0 | 643 | 54.3 | 690 | 30.3 | 737 | 43.7 |
| 597 | 0 | 644 | 55.2 | 691 | 30.9 | 738 | 44 |
| 598 | 0 | 645 | 55.5 | 692 | 31.1 | 739 | 44.1 |
| 599 | 0 | 646 | 55.9 | 693 | 31.8 | 740 | 45.3 |
| 600 | 0 | 647 | 56.3 | 694 | 32.7 | 741 | 46.4 |
| 601 | 1 | 648 | 56.7 | 695 | 33.2 | 742 | 47.2 |
| 602 | 2.1 | 649 | 56.9 | 696 | 32.4 | 743 | 47.3 |
| 603 | 5.2 | 650 | 56.8 | 697 | 28.3 | 744 | 47.4 |
| 604 | 9.2 | 651 | 56 | 698 | 25.8 | 745 | 47.4 |
| 605 | 13.5 | 652 | 54.2 | 699 | 23.1 | 746 | 47.5 |
| 606 | 18.1 | 653 | 52.1 | 700 | 21.8 | 747 | 47.9 |
| 607 | 22.3 | 654 | 50.1 | 701 | 21.2 | 748 | 48.6 |
| 608 | 26 | 655 | 47.2 | 702 | 21 | 749 | 49.4 |
| 609 | 29.3 | 656 | 43.2 | 703 | 21 | 750 | 49.8 |
| 610 | 32.8 | 657 | 39.2 | 704 | 20.9 | 751 | 49.8 |
| 611 | 36 | 658 | 36.5 | 705 | 19.9 | 752 | 49.7 |
| 612 | 39.2 | 659 | 34.3 | 706 | 17.9 | 753 | 49.3 |
| 613 | 42.5 | 660 | 31 | 707 | 15.1 | 754 | 48.5 |
| 614 | 45.7 | 661 | 26 | 708 | 12.8 | 755 | 47.6 |
| 615 | 48.2 | 662 | 20.7 | 709 | 12 | 756 | 46.3 |
| 616 | 48.4 | 663 | 15.4 | 710 | 13.2 | 757 | 43.7 |
| 617 | 48.2 | 664 | 13.1 | 711 | 17.1 | 758 | 39.3 |
| 618 | 47.8 | 665 | 12 | 712 | 21.1 | 759 | 34.1 |
| 619 | 47 | 666 | 12.5 | 713 | 21.8 | 760 | 29 |
| 620 | 45.9 | 667 | 14 | 714 | 21.2 | 761 | 23.7 |
| 621 | 44.9 | 668 | 19 | 715 | 18.5 | 762 | 18.4 |
| 622 | 44.4 | 669 | 23.2 | 716 | 13.9 | 763 | 14.3 |
| 623 | 44.3 | 670 | 28 | 717 | 12 | 764 | 12 |
| 624 | 44.5 | 671 | 32 | 718 | 12 | 765 | 12.8 |
| 625 | 45.1 | 672 | 34 | 719 | 13 | 766 | 16 |
| 626 | 45.7 | 673 | 36 | 720 | 16.3 | 767 | 20.4 |
| 627 | 46 | 674 | 38 | 721 | 20.5 | 768 | 24 |
| 628 | 46 | 675 | 40 | 722 | 23.9 | 769 | 29 |
| 629 | 46 | 676 | 40.3 | 723 | 26 | 770 | 32.2 |
| 630 | 46.1 | 677 | 40.5 | 724 | 28 | 771 | 36.8 |
| 631 | 46.7 | 678 | 39 | 725 | 31.5 | 772 | 39.4 |
| 632 | 47.7 | 679 | 35.7 | 726 | 33.4 | 773 | 43.2 |
| 633 | 48.9 | 680 | 31.8 | 727 | 36 | 774 | 45.8 |
| 634 | 50.3 | 681 | 27.1 | 728 | 37.8 | 775 | 49.2 |
| 635 | 51.6 | 682 | 22.8 | 729 | 40.2 | 776 | 51.4 |
| 636 | 52.6 | 683 | 21.1 | 730 | 41.6 | 777 | 54.2 |


| Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 778 | 56 | 827 | 37.1 | 876 | 75.8 | 925 | 62.3 |
| 779 | 58.3 | 828 | 38.9 | 877 | 76.6 | 926 | 62.7 |
| 780 | 59.8 | 829 | 41.4 | 878 | 76.5 | 927 | 62 |
| 781 | 61.7 | 830 | 44 | 879 | 76.2 | 928 | 61.3 |
| 782 | 62.7 | 831 | 46.3 | 880 | 75.8 | 929 | 60.9 |
| 783 | 63.3 | 832 | 47.7 | 881 | 75.4 | 930 | 60.5 |
| 784 | 63.6 | 833 | 48.2 | 882 | 74.8 | 931 | 60.2 |
| 785 | 64 | 834 | 48.7 | 883 | 73.9 | 932 | 59.8 |
| 786 | 64.7 | 835 | 49.3 | 884 | 72.7 | 933 | 59.4 |
| 787 | 65.2 | 836 | 49.8 | 885 | 71.3 | 934 | 58.6 |
| 788 | 65.3 | 837 | 50.2 | 886 | 70.4 | 935 | 57.5 |
| 789 | 65.3 | 838 | 50.9 | 887 | 70 | 936 | 56.6 |
| 790 | 65.4 | 839 | 51.8 | 888 | 70 | 937 | 56 |
| 791 | 65.7 | 840 | 52.5 | 889 | 69 | 938 | 55.5 |
| 792 | 66 | 841 | 53.3 | 890 | 68 | 939 | 55 |
| 793 | 65.6 | 842 | 54.5 | 891 | 67.3 | 940 | 54.4 |
| 794 | 63.5 | 843 | 55.7 | 892 | 66.2 | 941 | 54.1 |
| 795 | 59.7 | 844 | 56.5 | 893 | 64.8 | 942 | 54 |
| 796 | 54.6 | 845 | 56.8 | 894 | 63.6 | 943 | 53.9 |
| 797 | 49.3 | 846 | 57 | 895 | 62.6 | 944 | 53.9 |
| 798 | 44.9 | 847 | 57.2 | 896 | 62.1 | 945 | 54 |
| 799 | 42.3 | 848 | 57.7 | 897 | 61.9 | 946 | 54.2 |
| 800 | 41.4 | 849 | 58.7 | 898 | 61.9 | 947 | 55 |
| 801 | 41.3 | 850 | 60.1 | 899 | 61.8 | 948 | 55.8 |
| 802 | 43 | 851 | 61.1 | 900 | 61.5 | 949 | 56.2 |
| 803 | 45 | 852 | 61.7 | 901 | 60.9 | 950 | 56.1 |
| 804 | 46.5 | 853 | 62.3 | 902 | 59.7 | 951 | 55.1 |
| 805 | 48.3 | 854 | 62.9 | 903 | 54.6 | 952 | 52.7 |
| 806 | 49.5 | 855 | 63.3 | 904 | 49.3 | 953 | 48.4 |
| 807 | 51.2 | 856 | 63.4 | 905 | 44.9 | 954 | 43.1 |
| 808 | 52.2 | 857 | 63.5 | 906 | 42.3 | 955 | 37.8 |
| 809 | 51.6 | 858 | 63.9 | 907 | 41.4 | 956 | 32.5 |
| 810 | 49.7 | 859 | 64.4 | 908 | 41.3 | 957 | 27.2 |
| 811 | 47.4 | 860 | 65 | 909 | 42.1 | 958 | 25.1 |
| 812 | 43.7 | 861 | 65.6 | 910 | 44.7 | 959 | 27 |
| 813 | 39.7 | 862 | 66.6 | 911 | 46 | 960 | 29.8 |
| 814 | 35.5 | 863 | 67.4 | 912 | 48.8 | 961 | 33.8 |
| 815 | 31.1 | 864 | 68.2 | 913 | 50.1 | 962 | 37 |
| 816 | 26.3 | 865 | 69.1 | 914 | 51.3 | 963 | 40.7 |
| 817 | 21.9 | 866 | 70 | 915 | 54.1 | 964 | 43 |
| 818 | 18 | 867 | 70.8 | 916 | 55.2 | 965 | 45.6 |
| 819 | 17 | 868 | 71.5 | 917 | 56.2 | 966 | 46.9 |
| 820 | 18 | 869 | 72.4 | 918 | 56.1 | 967 | 47 |
| 821 | 21.4 | 870 | 73 | 919 | 56.1 | 968 | 46.9 |
| 822 | 24.8 | 871 | 73.7 | 920 | 56.5 | 969 | 46.5 |
| 823 | 27.9 | 872 | 74.4 | 921 | 57.5 | 970 | 45.8 |
| 824 | 30.8 | 873 | 74.9 | 922 | 59.2 | 971 | 44.3 |
| 825 | 33 | 874 | 75.3 | 923 | 60.7 | 972 | 41.3 |
| 826 | 35.1 | 875 | 75.6 | 924 | 61.8 | 973 | 36.5 |


| Time in $s$ | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in $s$ | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 974 | 31.7 |  |  |  |  |  |  |
| 975 | 27 |  |  |  |  |  |  |
| 976 | 24.7 |  |  |  |  |  |  |
| 977 | 19.3 |  |  |  |  |  |  |
| 978 | 16 |  |  |  |  |  |  |
| 979 | 13.2 |  |  |  |  |  |  |
| 980 | 10.7 |  |  |  |  |  |  |
| 981 | 8.8 |  |  |  |  |  |  |
| 982 | 7.2 |  |  |  |  |  |  |
| 983 | 5.5 |  |  |  |  |  |  |
| 984 | 3.2 |  |  |  |  |  |  |
| 985 | 1.1 |  |  |  |  |  |  |
| 986 | 0 |  |  |  |  |  |  |
| 987 | 0 |  |  |  |  |  |  |
| 988 | 0 |  |  |  |  |  |  |
| 989 | 0 |  |  |  |  |  |  |
| 990 | 0 |  |  |  |  |  |  |
| 991 | 0 |  |  |  |  |  |  |
| 992 | 0 |  |  |  |  |  |  |
| 993 | 0 |  |  |  |  |  |  |
| 994 | 0 |  |  |  |  |  |  |
| 995 | 0 |  |  |  |  |  |  |
| 996 | 0 |  |  |  |  |  |  |
| 997 | 0 |  |  |  |  |  |  |
| 998 | 0 |  |  |  |  |  |  |
| 999 | 0 |  |  |  |  |  |  |
| 1000 | 0 |  |  |  |  |  |  |
| 1001 | 0 |  |  |  |  |  |  |
| 1002 | 0 |  |  |  |  |  |  |
| 1003 | 0 |  |  |  |  |  |  |
| 1004 | 0 |  |  |  |  |  |  |
| 1005 | 0 |  |  |  |  |  |  |
| 1006 | 0 |  |  |  |  |  |  |
| 1007 | 0 |  |  |  |  |  |  |
| 1008 | 0 |  |  |  |  |  |  |
| 1009 | 0 |  |  |  |  |  |  |
| 1010 | 0 |  |  |  |  |  |  |
| 1011 | 0 |  |  |  |  |  |  |
| 1012 | 0 |  |  |  |  |  |  |
| 1013 | 0 |  |  |  |  |  |  |
| 1014 | 0 |  |  |  |  |  |  |
| 1015 | 0 |  |  |  |  |  |  |
| 1016 | 0 |  |  |  |  |  |  |
| 1017 | 0 |  |  |  |  |  |  |
| 1018 | 0 |  |  |  |  |  |  |
| 1019 | 0 |  |  |  |  |  |  |
| 1020 | 0 |  |  |  |  |  |  |
| 1021 | 0 |  |  |  |  |  |  |
| 1022 | 0 |  |  |  |  |  |  |

Table A/9
WLTC, Class 3 vehicles of which maximum speed is higher than $120 \mathrm{~km} / \mathrm{h}$, phase Medium

| Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 590 | 0 | 637 | 53 | 684 | 18.9 | 731 | 41.9 |
| 591 | 0 | 638 | 53 | 685 | 18.9 | 732 | 42 |
| 592 | 0 | 639 | 52.9 | 686 | 21.3 | 733 | 42.2 |
| 593 | 0 | 640 | 52.7 | 687 | 23.9 | 734 | 42.4 |
| 594 | 0 | 641 | 52.6 | 688 | 25.9 | 735 | 42.7 |
| 595 | 0 | 642 | 53.1 | 689 | 28.4 | 736 | 43.1 |
| 596 | 0 | 643 | 54.3 | 690 | 30.3 | 737 | 43.7 |
| 597 | 0 | 644 | 55.2 | 691 | 30.9 | 738 | 44 |
| 598 | 0 | 645 | 55.5 | 692 | 31.1 | 739 | 44.1 |
| 599 | 0 | 646 | 55.9 | 693 | 31.8 | 740 | 45.3 |
| 600 | 0 | 647 | 56.3 | 694 | 32.7 | 741 | 46.4 |
| 601 | 1 | 648 | 56.7 | 695 | 33.2 | 742 | 47.2 |
| 602 | 2.1 | 649 | 56.9 | 696 | 32.4 | 743 | 47.3 |
| 603 | 4.8 | 650 | 56.8 | 697 | 28.3 | 744 | 47.4 |
| 604 | 9.1 | 651 | 56 | 698 | 25.8 | 745 | 47.4 |
| 605 | 14.2 | 652 | 54.2 | 699 | 23.1 | 746 | 47.5 |
| 606 | 19.8 | 653 | 52.1 | 700 | 21.8 | 747 | 47.9 |
| 607 | 25.5 | 654 | 50.1 | 701 | 21.2 | 748 | 48.6 |
| 608 | 30.5 | 655 | 47.2 | 702 | 21 | 749 | 49.4 |
| 609 | 34.8 | 656 | 43.2 | 703 | 21 | 750 | 49.8 |
| 610 | 38.8 | 657 | 39.2 | 704 | 20.9 | 751 | 49.8 |
| 611 | 42.9 | 658 | 36.5 | 705 | 19.9 | 752 | 49.7 |
| 612 | 46.4 | 659 | 34.3 | 706 | 17.9 | 753 | 49.3 |
| 613 | 48.3 | 660 | 31 | 707 | 15.1 | 754 | 48.5 |
| 614 | 48.7 | 661 | 26 | 708 | 12.8 | 755 | 47.6 |
| 615 | 48.5 | 662 | 20.7 | 709 | 12 | 756 | 46.3 |
| 616 | 48.4 | 663 | 15.4 | 710 | 13.2 | 757 | 43.7 |
| 617 | 48.2 | 664 | 13.1 | 711 | 17.1 | 758 | 39.3 |
| 618 | 47.8 | 665 | 12 | 712 | 21.1 | 759 | 34.1 |
| 619 | 47 | 666 | 12.5 | 713 | 21.8 | 760 | 29 |
| 620 | 45.9 | 667 | 14 | 714 | 21.2 | 761 | 23.7 |
| 621 | 44.9 | 668 | 19 | 715 | 18.5 | 762 | 18.4 |
| 622 | 44.4 | 669 | 23.2 | 716 | 13.9 | 763 | 14.3 |
| 623 | 44.3 | 670 | 28 | 717 | 12 | 764 | 12 |
| 624 | 44.5 | 671 | 32 | 718 | 12 | 765 | 12.8 |
| 625 | 45.1 | 672 | 34 | 719 | 13 | 766 | 16 |
| 626 | 45.7 | 673 | 36 | 720 | 16 | 767 | 19.1 |
| 627 | 46 | 674 | 38 | 721 | 18.5 | 768 | 22.4 |
| 628 | 46 | 675 | 40 | 722 | 20.6 | 769 | 25.6 |
| 629 | 46 | 676 | 40.3 | 723 | 22.5 | 770 | 30.1 |
| 630 | 46.1 | 677 | 40.5 | 724 | 24 | 771 | 35.3 |
| 631 | 46.7 | 678 | 39 | 725 | 26.6 | 772 | 39.9 |
| 632 | 47.7 | 679 | 35.7 | 726 | 29.9 | 773 | 44.5 |
| 633 | 48.9 | 680 | 31.8 | 727 | 34.8 | 774 | 47.5 |
| 634 | 50.3 | 681 | 27.1 | 728 | 37.8 | 775 | 50.9 |
| 635 | 51.6 | 682 | 22.8 | 729 | 40.2 | 776 | 54.1 |
| 636 | 52.6 | 683 | 21.1 | 730 | 41.6 | 777 | 56.3 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 778 | 58.1 | 827 | 37.1 | 876 | 72.7 | 925 | 64.1 |
| 779 | 59.8 | 828 | 38.9 | 877 | 71.3 | 926 | 62.7 |
| 780 | 61.1 | 829 | 41.4 | 878 | 70.4 | 927 | 62 |
| 781 | 62.1 | 830 | 44 | 879 | 70 | 928 | 61.3 |
| 782 | 62.8 | 831 | 46.3 | 880 | 70 | 929 | 60.9 |
| 783 | 63.3 | 832 | 47.7 | 881 | 69 | 930 | 60.5 |
| 784 | 63.6 | 833 | 48.2 | 882 | 68 | 931 | 60.2 |
| 785 | 64 | 834 | 48.7 | 883 | 68 | 932 | 59.8 |
| 786 | 64.7 | 835 | 49.3 | 884 | 68 | 933 | 59.4 |
| 787 | 65.2 | 836 | 49.8 | 885 | 68.1 | 934 | 58.6 |
| 788 | 65.3 | 837 | 50.2 | 886 | 68.4 | 935 | 57.5 |
| 789 | 65.3 | 838 | 50.9 | 887 | 68.6 | 936 | 56.6 |
| 790 | 65.4 | 839 | 51.8 | 888 | 68.7 | 937 | 56 |
| 791 | 65.7 | 840 | 52.5 | 889 | 68.5 | 938 | 55.5 |
| 792 | 66 | 841 | 53.3 | 890 | 68.1 | 939 | 55 |
| 793 | 65.6 | 842 | 54.5 | 891 | 67.3 | 940 | 54.4 |
| 794 | 63.5 | 843 | 55.7 | 892 | 66.2 | 941 | 54.1 |
| 795 | 59.7 | 844 | 56.5 | 893 | 64.8 | 942 | 54 |
| 796 | 54.6 | 845 | 56.8 | 894 | 63.6 | 943 | 53.9 |
| 797 | 49.3 | 846 | 57 | 895 | 62.6 | 944 | 53.9 |
| 798 | 44.9 | 847 | 57.2 | 896 | 62.1 | 945 | 54 |
| 799 | 42.3 | 848 | 57.7 | 897 | 61.9 | 946 | 54.2 |
| 800 | 41.4 | 849 | 58.7 | 898 | 61.9 | 947 | 55 |
| 801 | 41.3 | 850 | 60.1 | 899 | 61.8 | 948 | 55.8 |
| 802 | 42.1 | 851 | 61.1 | 900 | 61.5 | 949 | 56.2 |
| 803 | 44.7 | 852 | 61.7 | 901 | 60.9 | 950 | 56.1 |
| 804 | 48.4 | 853 | 62.3 | 902 | 59.7 | 951 | 55.1 |
| 805 | 51.4 | 854 | 62.9 | 903 | 54.6 | 952 | 52.7 |
| 806 | 52.7 | 855 | 63.3 | 904 | 49.3 | 953 | 48.4 |
| 807 | 53 | 856 | 63.4 | 905 | 44.9 | 954 | 43.1 |
| 808 | 52.5 | 857 | 63.5 | 906 | 42.3 | 955 | 37.8 |
| 809 | 51.3 | 858 | 64.5 | 907 | 41.4 | 956 | 32.5 |
| 810 | 49.7 | 859 | 65.8 | 908 | 41.3 | 957 | 27.2 |
| 811 | 47.4 | 860 | 66.8 | 909 | 42.1 | 958 | 25.1 |
| 812 | 43.7 | 861 | 67.4 | 910 | 44.7 | 959 | 26 |
| 813 | 39.7 | 862 | 68.8 | 911 | 48.4 | 960 | 29.3 |
| 814 | 35.5 | 863 | 71.1 | 912 | 51.4 | 961 | 34.6 |
| 815 | 31.1 | 864 | 72.3 | 913 | 52.7 | 962 | 40.4 |
| 816 | 26.3 | 865 | 72.8 | 914 | 54 | 963 | 45.3 |
| 817 | 21.9 | 866 | 73.4 | 915 | 57 | 964 | 49 |
| 818 | 18 | 867 | 74.6 | 916 | 58.1 | 965 | 51.1 |
| 819 | 17 | 868 | 76 | 917 | 59.2 | 966 | 52.1 |
| 820 | 18 | 869 | 76.6 | 918 | 59 | 967 | 52.2 |
| 821 | 21.4 | 870 | 76.5 | 919 | 59.1 | 968 | 52.1 |
| 822 | 24.8 | 871 | 76.2 | 920 | 59.5 | 969 | 51.7 |
| 823 | 27.9 | 872 | 75.8 | 921 | 60.5 | 970 | 50.9 |
| 824 | 30.8 | 873 | 75.4 | 922 | 62.3 | 971 | 49.2 |
| 825 | 33 | 874 | 74.8 | 923 | 63.9 | 972 | 45.9 |
| 826 | 35.1 | 875 | 73.9 | 924 | 65.1 | 973 | 40.6 |


| Time in $s$ | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in $s$ | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 974 | 35.3 |  |  |  |  |  |  |
| 975 | 30 |  |  |  |  |  |  |
| 976 | 24.7 |  |  |  |  |  |  |
| 977 | 19.3 |  |  |  |  |  |  |
| 978 | 16 |  |  |  |  |  |  |
| 979 | 13.2 |  |  |  |  |  |  |
| 980 | 10.7 |  |  |  |  |  |  |
| 981 | 8.8 |  |  |  |  |  |  |
| 982 | 7.2 |  |  |  |  |  |  |
| 983 | 5.5 |  |  |  |  |  |  |
| 984 | 3.2 |  |  |  |  |  |  |
| 985 | 1.1 |  |  |  |  |  |  |
| 986 | 0 |  |  |  |  |  |  |
| 987 | 0 |  |  |  |  |  |  |
| 988 | 0 |  |  |  |  |  |  |
| 989 | 0 |  |  |  |  |  |  |
| 990 | 0 |  |  |  |  |  |  |
| 991 | 0 |  |  |  |  |  |  |
| 992 | 0 |  |  |  |  |  |  |
| 993 | 0 |  |  |  |  |  |  |
| 994 | 0 |  |  |  |  |  |  |
| 995 | 0 |  |  |  |  |  |  |
| 996 | 0 |  |  |  |  |  |  |
| 997 | 0 |  |  |  |  |  |  |
| 998 | 0 |  |  |  |  |  |  |
| 999 | 0 |  |  |  |  |  |  |
| 1000 | 0 |  |  |  |  |  |  |
| 1001 | 0 |  |  |  |  |  |  |
| 1002 | 0 |  |  |  |  |  |  |
| 1003 | 0 |  |  |  |  |  |  |
| 1004 | 0 |  |  |  |  |  |  |
| 1005 | 0 |  |  |  |  |  |  |
| 1006 | 0 |  |  |  |  |  |  |
| 1007 | 0 |  |  |  |  |  |  |
| 1008 | 0 |  |  |  |  |  |  |
| 1009 | 0 |  |  |  |  |  |  |
| 1010 | 0 |  |  |  |  |  |  |
| 1011 | 0 |  |  |  |  |  |  |
| 1012 | 0 |  |  |  |  |  |  |
| 1013 | 0 |  |  |  |  |  |  |
| 1014 | 0 |  |  |  |  |  |  |
| 1015 | 0 |  |  |  |  |  |  |
| 1016 | 0 |  |  |  |  |  |  |
| 1017 | 0 |  |  |  |  |  |  |
| 1018 | 0 |  |  |  |  |  |  |
| 1019 | 0 |  |  |  |  |  |  |
| 1020 | 0 |  |  |  |  |  |  |
| 1021 | 0 |  |  |  |  |  |  |
| 1022 | 0 |  |  |  |  |  |  |

Table A/10
WLTC, Class 3 vehicles of which maximum speed is less than $120 \mathrm{~km} / \mathrm{h}$, phase High

| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1023 | 0 | 1070 | 29 | 1117 | 66.2 | 1164 | 52.6 |
| 1024 | 0 | 1071 | 32 | 1118 | 65.8 | 1165 | 54.5 |
| 1025 | 0 | 1072 | 34.8 | 1119 | 64.7 | 1166 | 56.6 |
| 1026 | 0 | 1073 | 37.7 | 1120 | 63.6 | 1167 | 58.3 |
| 1027 | 0.8 | 1074 | 40.8 | 1121 | 62.9 | 1168 | 60 |
| 1028 | 3.6 | 1075 | 43.2 | 1122 | 62.4 | 1169 | 61.5 |
| 1029 | 8.6 | 1076 | 46 | 1123 | 61.7 | 1170 | 63.1 |
| 1030 | 14.6 | 1077 | 48 | 1124 | 60.1 | 1171 | 64.3 |
| 1031 | 20 | 1078 | 50.7 | 1125 | 57.3 | 1172 | 65.7 |
| 1032 | 24.4 | 1079 | 52 | 1126 | 55.8 | 1173 | 67.1 |
| 1033 | 28.2 | 1080 | 54.5 | 1127 | 50.5 | 1174 | 68.3 |
| 1034 | 31.7 | 1081 | 55.9 | 1128 | 45.2 | 1175 | 69.7 |
| 1035 | 35 | 1082 | 57.4 | 1129 | 40.1 | 1176 | 70.6 |
| 1036 | 37.6 | 1083 | 58.1 | 1130 | 36.2 | 1177 | 71.6 |
| 1037 | 39.7 | 1084 | 58.4 | 1131 | 32.9 | 1178 | 72.6 |
| 1038 | 41.5 | 1085 | 58.8 | 1132 | 29.8 | 1179 | 73.5 |
| 1039 | 43.6 | 1086 | 58.8 | 1133 | 26.6 | 1180 | 74.2 |
| 1040 | 46 | 1087 | 58.6 | 1134 | 23 | 1181 | 74.9 |
| 1041 | 48.4 | 1088 | 58.7 | 1135 | 19.4 | 1182 | 75.6 |
| 1042 | 50.5 | 1089 | 58.8 | 1136 | 16.3 | 1183 | 76.3 |
| 1043 | 51.9 | 1090 | 58.8 | 1137 | 14.6 | 1184 | 77.1 |
| 1044 | 52.6 | 1091 | 58.8 | 1138 | 14.2 | 1185 | 77.9 |
| 1045 | 52.8 | 1092 | 59.1 | 1139 | 14.3 | 1186 | 78.5 |
| 1046 | 52.9 | 1093 | 60.1 | 1140 | 14.6 | 1187 | 79 |
| 1047 | 53.1 | 1094 | 61.7 | 1141 | 15.1 | 1188 | 79.7 |
| 1048 | 53.3 | 1095 | 63 | 1142 | 16.4 | 1189 | 80.3 |
| 1049 | 53.1 | 1096 | 63.7 | 1143 | 19.1 | 1190 | 81 |
| 1050 | 52.3 | 1097 | 63.9 | 1144 | 22.5 | 1191 | 81.6 |
| 1051 | 50.7 | 1098 | 63.5 | 1145 | 24.4 | 1192 | 82.4 |
| 1052 | 48.8 | 1099 | 62.3 | 1146 | 24.8 | 1193 | 82.9 |
| 1053 | 46.5 | 1100 | 60.3 | 1147 | 22.7 | 1194 | 83.4 |
| 1054 | 43.8 | 1101 | 58.9 | 1148 | 17.4 | 1195 | 83.8 |
| 1055 | 40.3 | 1102 | 58.4 | 1149 | 13.8 | 1196 | 84.2 |
| 1056 | 36 | 1103 | 58.8 | 1150 | 12 | 1197 | 84.7 |
| 1057 | 30.7 | 1104 | 60.2 | 1151 | 12 | 1198 | 85.2 |
| 1058 | 25.4 | 1105 | 62.3 | 1152 | 12 | 1199 | 85.6 |
| 1059 | 21 | 1106 | 63.9 | 1153 | 13.9 | 1200 | 86.3 |
| 1060 | 16.7 | 1107 | 64.5 | 1154 | 17.7 | 1201 | 86.8 |
| 1061 | 13.4 | 1108 | 64.4 | 1155 | 22.8 | 1202 | 87.4 |
| 1062 | 12 | 1109 | 63.5 | 1156 | 27.3 | 1203 | 88 |
| 1063 | 12.1 | 1110 | 62 | 1157 | 31.2 | 1204 | 88.3 |
| 1064 | 12.8 | 1111 | 61.2 | 1158 | 35.2 | 1205 | 88.7 |
| 1065 | 15.6 | 1112 | 61.3 | 1159 | 39.4 | 1206 | 89 |
| 1066 | 19.9 | 1113 | 61.7 | 1160 | 42.5 | 1207 | 89.3 |
| 1067 | 23.4 | 1114 | 62 | 1161 | 45.4 | 1208 | 89.8 |
| 1068 | 24.6 | 1115 | 64.6 | 1162 | 48.2 | 1209 | 90.2 |
| 1069 | 27 | 1116 | 66 | 1163 | 50.3 | 1210 | 90.6 |


| Time in s | speed in km/h | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1211 | 91 | 1260 | 95.7 | 1309 | 75.9 | 1358 | 68.2 |
| 1212 | 91.3 | 1261 | 95.5 | 1310 | 76 | 1359 | 66.1 |
| 1213 | 91.6 | 1262 | 95.3 | 1311 | 76 | 1360 | 63.8 |
| 1214 | 91.9 | 1263 | 95.2 | 1312 | 76.1 | 1361 | 61.6 |
| 1215 | 92.2 | 1264 | 95 | 1313 | 76.3 | 1362 | 60.2 |
| 1216 | 92.8 | 1265 | 94.9 | 1314 | 76.5 | 1363 | 59.8 |
| 1217 | 93.1 | 1266 | 94.7 | 1315 | 76.6 | 1364 | 60.4 |
| 1218 | 93.3 | 1267 | 94.5 | 1316 | 76.8 | 1365 | 61.8 |
| 1219 | 93.5 | 1268 | 94.4 | 1317 | 77.1 | 1366 | 62.6 |
| 1220 | 93.7 | 1269 | 94.4 | 1318 | 77.1 | 1367 | 62.7 |
| 1221 | 93.9 | 1270 | 94.3 | 1319 | 77.2 | 1368 | 61.9 |
| 1222 | 94 | 1271 | 94.3 | 1320 | 77.2 | 1369 | 60 |
| 1223 | 94.1 | 1272 | 94.1 | 1321 | 77.6 | 1370 | 58.4 |
| 1224 | 94.3 | 1273 | 93.9 | 1322 | 78 | 1371 | 57.8 |
| 1225 | 94.4 | 1274 | 93.4 | 1323 | 78.4 | 1372 | 57.8 |
| 1226 | 94.6 | 1275 | 92.8 | 1324 | 78.8 | 1373 | 57.8 |
| 1227 | 94.7 | 1276 | 92 | 1325 | 79.2 | 1374 | 57.3 |
| 1228 | 94.8 | 1277 | 91.3 | 1326 | 80.3 | 1375 | 56.2 |
| 1229 | 95 | 1278 | 90.6 | 1327 | 80.8 | 1376 | 54.3 |
| 1230 | 95.1 | 1279 | 90 | 1328 | 81 | 1377 | 50.8 |
| 1231 | 95.3 | 1280 | 89.3 | 1329 | 81 | 1378 | 45.5 |
| 1232 | 95.4 | 1281 | 88.7 | 1330 | 81 | 1379 | 40.2 |
| 1233 | 95.6 | 1282 | 88.1 | 1331 | 81 | 1380 | 34.9 |
| 1234 | 95.7 | 1283 | 87.4 | 1332 | 81 | 1381 | 29.6 |
| 1235 | 95.8 | 1284 | 86.7 | 1333 | 80.9 | 1382 | 28.7 |
| 1236 | 96 | 1285 | 86 | 1334 | 80.6 | 1383 | 29.3 |
| 1237 | 96.1 | 1286 | 85.3 | 1335 | 80.3 | 1384 | 30.5 |
| 1238 | 96.3 | 1287 | 84.7 | 1336 | 80 | 1385 | 31.7 |
| 1239 | 96.4 | 1288 | 84.1 | 1337 | 79.9 | 1386 | 32.9 |
| 1240 | 96.6 | 1289 | 83.5 | 1338 | 79.8 | 1387 | 35 |
| 1241 | 96.8 | 1290 | 82.9 | 1339 | 79.8 | 1388 | 38 |
| 1242 | 97 | 1291 | 82.3 | 1340 | 79.8 | 1389 | 40.5 |
| 1243 | 97.2 | 1292 | 81.7 | 1341 | 79.9 | 1390 | 42.7 |
| 1244 | 97.3 | 1293 | 81.1 | 1342 | 80 | 1391 | 45.8 |
| 1245 | 97.4 | 1294 | 80.5 | 1343 | 80.4 | 1392 | 47.5 |
| 1246 | 97.4 | 1295 | 79.9 | 1344 | 80.8 | 1393 | 48.9 |
| 1247 | 97.4 | 1296 | 79.4 | 1345 | 81.2 | 1394 | 49.4 |
| 1248 | 97.4 | 1297 | 79.1 | 1346 | 81.5 | 1395 | 49.4 |
| 1249 | 97.3 | 1298 | 78.8 | 1347 | 81.6 | 1396 | 49.2 |
| 1250 | 97.3 | 1299 | 78.5 | 1348 | 81.6 | 1397 | 48.7 |
| 1251 | 97.3 | 1300 | 78.2 | 1349 | 81.4 | 1398 | 47.9 |
| 1252 | 97.3 | 1301 | 77.9 | 1350 | 80.7 | 1399 | 46.9 |
| 1253 | 97.2 | 1302 | 77.6 | 1351 | 79.6 | 1400 | 45.6 |
| 1254 | 97.1 | 1303 | 77.3 | 1352 | 78.2 | 1401 | 44.2 |
| 1255 | 97 | 1304 | 77 | 1353 | 76.8 | 1402 | 42.7 |
| 1256 | 96.9 | 1305 | 76.7 | 1354 | 75.3 | 1403 | 40.7 |
| 1257 | 96.7 | 1306 | 76 | 1355 | 73.8 | 1404 | 37.1 |
| 1258 | 96.4 | 1307 | 76 | 1356 | 72.1 | 1405 | 33.9 |
| 1259 | 96.1 | 1308 | 76 | 1357 | 70.2 | 1406 | 30.6 |

Table A/11
WLTC, Class 3 vehicles of which maximum speed is higher than $120 \mathrm{~km} / \mathrm{h}$, phase High

| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1023 | 0 | 1070 | 26.4 | 1117 | 69.7 | 1164 | 52.6 |
| 1024 | 0 | 1071 | 28.8 | 1118 | 69.3 | 1165 | 54.5 |
| 1025 | 0 | 1072 | 31.8 | 1119 | 68.1 | 1166 | 56.6 |
| 1026 | 0 | 1073 | 35.3 | 1120 | 66.9 | 1167 | 58.3 |
| 1027 | 0.8 | 1074 | 39.5 | 1121 | 66.2 | 1168 | 60 |
| 1028 | 3.6 | 1075 | 44.5 | 1122 | 65.7 | 1169 | 61.5 |
| 1029 | 8.6 | 1076 | 49.3 | 1123 | 64.9 | 1170 | 63.1 |
| 1030 | 14.6 | 1077 | 53.3 | 1124 | 63.2 | 1171 | 64.3 |
| 1031 | 20 | 1078 | 56.4 | 1125 | 60.3 | 1172 | 65.7 |
| 1032 | 24.4 | 1079 | 58.9 | 1126 | 55.8 | 1173 | 67.1 |
| 1033 | 28.2 | 1080 | 61.2 | 1127 | 50.5 | 1174 | 68.3 |
| 1034 | 31.7 | 1081 | 62.6 | 1128 | 45.2 | 1175 | 69.7 |
| 1035 | 35 | 1082 | 63 | 1129 | 40.1 | 1176 | 70.6 |
| 1036 | 37.6 | 1083 | 62.5 | 1130 | 36.2 | 1177 | 71.6 |
| 1037 | 39.7 | 1084 | 60.9 | 1131 | 32.9 | 1178 | 72.6 |
| 1038 | 41.5 | 1085 | 59.3 | 1132 | 29.8 | 1179 | 73.5 |
| 1039 | 43.6 | 1086 | 58.6 | 1133 | 26.6 | 1180 | 74.2 |
| 1040 | 46 | 1087 | 58.6 | 1134 | 23 | 1181 | 74.9 |
| 1041 | 48.4 | 1088 | 58.7 | 1135 | 19.4 | 1182 | 75.6 |
| 1042 | 50.5 | 1089 | 58.8 | 1136 | 16.3 | 1183 | 76.3 |
| 1043 | 51.9 | 1090 | 58.8 | 1137 | 14.6 | 1184 | 77.1 |
| 1044 | 52.6 | 1091 | 58.8 | 1138 | 14.2 | 1185 | 77.9 |
| 1045 | 52.8 | 1092 | 59.1 | 1139 | 14.3 | 1186 | 78.5 |
| 1046 | 52.9 | 1093 | 60.1 | 1140 | 14.6 | 1187 | 79 |
| 1047 | 53.1 | 1094 | 61.7 | 1141 | 15.1 | 1188 | 79.7 |
| 1048 | 53.3 | 1095 | 63 | 1142 | 16.4 | 1189 | 80.3 |
| 1049 | 53.1 | 1096 | 63.7 | 1143 | 19.1 | 1190 | 81 |
| 1050 | 52.3 | 1097 | 63.9 | 1144 | 22.5 | 1191 | 81.6 |
| 1051 | 50.7 | 1098 | 63.5 | 1145 | 24.4 | 1192 | 82.4 |
| 1052 | 48.8 | 1099 | 62.3 | 1146 | 24.8 | 1193 | 82.9 |
| 1053 | 46.5 | 1100 | 60.3 | 1147 | 22.7 | 1194 | 83.4 |
| 1054 | 43.8 | 1101 | 58.9 | 1148 | 17.4 | 1195 | 83.8 |
| 1055 | 40.3 | 1102 | 58.4 | 1149 | 13.8 | 1196 | 84.2 |
| 1056 | 36 | 1103 | 58.8 | 1150 | 12 | 1197 | 84.7 |
| 1057 | 30.7 | 1104 | 60.2 | 1151 | 12 | 1198 | 85.2 |
| 1058 | 25.4 | 1105 | 62.3 | 1152 | 12 | 1199 | 85.6 |
| 1059 | 21 | 1106 | 63.9 | 1153 | 13.9 | 1200 | 86.3 |
| 1060 | 16.7 | 1107 | 64.5 | 1154 | 17.7 | 1201 | 86.8 |
| 1061 | 13.4 | 1108 | 64.4 | 1155 | 22.8 | 1202 | 87.4 |
| 1062 | 12 | 1109 | 63.5 | 1156 | 27.3 | 1203 | 88 |
| 1063 | 12.1 | 1110 | 62 | 1157 | 31.2 | 1204 | 88.3 |
| 1064 | 12.8 | 1111 | 61.2 | 1158 | 35.2 | 1205 | 88.7 |
| 1065 | 15.6 | 1112 | 61.3 | 1159 | 39.4 | 1206 | 89 |
| 1066 | 19.9 | 1113 | 62.6 | 1160 | 42.5 | 1207 | 89.3 |
| 1067 | 23.4 | 1114 | 65.3 | 1161 | 45.4 | 1208 | 89.8 |
| 1068 | 24.6 | 1115 | 68 | 1162 | 48.2 | 1209 | 90.2 |
| 1069 | 25.2 | 1116 | 69.4 | 1163 | 50.3 | 1210 | 90.6 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1211 | 91 | 1260 | 95.7 | 1309 | 75.9 | 1358 | 68.2 |
| 1212 | 91.3 | 1261 | 95.5 | 1310 | 75.9 | 1359 | 66.1 |
| 1213 | 91.6 | 1262 | 95.3 | 1311 | 75.8 | 1360 | 63.8 |
| 1214 | 91.9 | 1263 | 95.2 | 1312 | 75.7 | 1361 | 61.6 |
| 1215 | 92.2 | 1264 | 95 | 1313 | 75.5 | 1362 | 60.2 |
| 1216 | 92.8 | 1265 | 94.9 | 1314 | 75.2 | 1363 | 59.8 |
| 1217 | 93.1 | 1266 | 94.7 | 1315 | 75 | 1364 | 60.4 |
| 1218 | 93.3 | 1267 | 94.5 | 1316 | 74.7 | 1365 | 61.8 |
| 1219 | 93.5 | 1268 | 94.4 | 1317 | 74.1 | 1366 | 62.6 |
| 1220 | 93.7 | 1269 | 94.4 | 1318 | 73.7 | 1367 | 62.7 |
| 1221 | 93.9 | 1270 | 94.3 | 1319 | 73.3 | 1368 | 61.9 |
| 1222 | 94 | 1271 | 94.3 | 1320 | 73.5 | 1369 | 60 |
| 1223 | 94.1 | 1272 | 94.1 | 1321 | 74 | 1370 | 58.4 |
| 1224 | 94.3 | 1273 | 93.9 | 1322 | 74.9 | 1371 | 57.8 |
| 1225 | 94.4 | 1274 | 93.4 | 1323 | 76.1 | 1372 | 57.8 |
| 1226 | 94.6 | 1275 | 92.8 | 1324 | 77.7 | 1373 | 57.8 |
| 1227 | 94.7 | 1276 | 92 | 1325 | 79.2 | 1374 | 57.3 |
| 1228 | 94.8 | 1277 | 91.3 | 1326 | 80.3 | 1375 | 56.2 |
| 1229 | 95 | 1278 | 90.6 | 1327 | 80.8 | 1376 | 54.3 |
| 1230 | 95.1 | 1279 | 90 | 1328 | 81 | 1377 | 50.8 |
| 1231 | 95.3 | 1280 | 89.3 | 1329 | 81 | 1378 | 45.5 |
| 1232 | 95.4 | 1281 | 88.7 | 1330 | 81 | 1379 | 40.2 |
| 1233 | 95.6 | 1282 | 88.1 | 1331 | 81 | 1380 | 34.9 |
| 1234 | 95.7 | 1283 | 87.4 | 1332 | 81 | 1381 | 29.6 |
| 1235 | 95.8 | 1284 | 86.7 | 1333 | 80.9 | 1382 | 27.3 |
| 1236 | 96 | 1285 | 86 | 1334 | 80.6 | 1383 | 29.3 |
| 1237 | 96.1 | 1286 | 85.3 | 1335 | 80.3 | 1384 | 32.9 |
| 1238 | 96.3 | 1287 | 84.7 | 1336 | 80 | 1385 | 35.6 |
| 1239 | 96.4 | 1288 | 84.1 | 1337 | 79.9 | 1386 | 36.7 |
| 1240 | 96.6 | 1289 | 83.5 | 1338 | 79.8 | 1387 | 37.6 |
| 1241 | 96.8 | 1290 | 82.9 | 1339 | 79.8 | 1388 | 39.4 |
| 1242 | 97 | 1291 | 82.3 | 1340 | 79.8 | 1389 | 42.5 |
| 1243 | 97.2 | 1292 | 81.7 | 1341 | 79.9 | 1390 | 46.5 |
| 1244 | 97.3 | 1293 | 81.1 | 1342 | 80 | 1391 | 50.2 |
| 1245 | 97.4 | 1294 | 80.5 | 1343 | 80.4 | 1392 | 52.8 |
| 1246 | 97.4 | 1295 | 79.9 | 1344 | 80.8 | 1393 | 54.3 |
| 1247 | 97.4 | 1296 | 79.4 | 1345 | 81.2 | 1394 | 54.9 |
| 1248 | 97.4 | 1297 | 79.1 | 1346 | 81.5 | 1395 | 54.9 |
| 1249 | 97.3 | 1298 | 78.8 | 1347 | 81.6 | 1396 | 54.7 |
| 1250 | 97.3 | 1299 | 78.5 | 1348 | 81.6 | 1397 | 54.1 |
| 1251 | 97.3 | 1300 | 78.2 | 1349 | 81.4 | 1398 | 53.2 |
| 1252 | 97.3 | 1301 | 77.9 | 1350 | 80.7 | 1399 | 52.1 |
| 1253 | 97.2 | 1302 | 77.6 | 1351 | 79.6 | 1400 | 50.7 |
| 1254 | 97.1 | 1303 | 77.3 | 1352 | 78.2 | 1401 | 49.1 |
| 1255 | 97 | 1304 | 77 | 1353 | 76.8 | 1402 | 47.4 |
| 1256 | 96.9 | 1305 | 76.7 | 1354 | 75.3 | 1403 | 45.2 |
| 1257 | 96.7 | 1306 | 76 | 1355 | 73.8 | 1404 | 41.8 |
| 1258 | 96.4 | 1307 | 76 | 1356 | 72.1 | 1405 | 36.5 |
| 1259 | 96.1 | 1308 | 76 | 1357 | 70.2 | 1406 | 31.2 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1407 | 27.6 | 1456 | 0 |  |  |  |  |
| 1408 | 26.9 | 1457 | 0 |  |  |  |  |
| 1409 | 27.3 | 1458 | 0 |  |  |  |  |
| 1410 | 27.5 | 1459 | 0 |  |  |  |  |
| 1411 | 27.4 | 1460 | 0 |  |  |  |  |
| 1412 | 27.1 | 1461 | 0 |  |  |  |  |
| 1413 | 26.7 | 1462 | 0 |  |  |  |  |
| 1414 | 26.8 | 1463 | 0 |  |  |  |  |
| 1415 | 28.2 | 1464 | 0 |  |  |  |  |
| 1416 | 31.1 | 1465 | 0 |  |  |  |  |
| 1417 | 34.8 | 1466 | 0 |  |  |  |  |
| 1418 | 38.4 | 1467 | 0 |  |  |  |  |
| 1419 | 40.9 | 1468 | 0 |  |  |  |  |
| 1420 | 41.7 | 1469 | 0 |  |  |  |  |
| 1421 | 40.9 | 1470 | 0 |  |  |  |  |
| 1422 | 38.3 | 1471 | 0 |  |  |  |  |
| 1423 | 35.3 | 1472 | 0 |  |  |  |  |
| 1424 | 34.3 | 1473 | 0 |  |  |  |  |
| 1425 | 34.6 | 1474 | 0 |  |  |  |  |
| 1426 | 36.3 | 1475 | 0 |  |  |  |  |
| 1427 | 39.5 | 1476 | 0 |  |  |  |  |
| 1428 | 41.8 | 1477 | 0 |  |  |  |  |
| 1429 | 42.5 |  |  |  |  |  |  |
| 1430 | 41.9 |  |  |  |  |  |  |
| 1431 | 40.1 |  |  |  |  |  |  |
| 1432 | 36.6 |  |  |  |  |  |  |
| 1433 | 31.3 |  |  |  |  |  |  |
| 1434 | 26 |  |  |  |  |  |  |
| 1435 | 20.6 |  |  |  |  |  |  |
| 1436 | 19.1 |  |  |  |  |  |  |
| 1437 | 19.7 |  |  |  |  |  |  |
| 1438 | 21.1 |  |  |  |  |  |  |
| 1439 | 22 |  |  |  |  |  |  |
| 1440 | 22.1 |  |  |  |  |  |  |
| 1441 | 21.4 |  |  |  |  |  |  |
| 1442 | 19.6 |  |  |  |  |  |  |
| 1443 | 18.3 |  |  |  |  |  |  |
| 1444 | 18 |  |  |  |  |  |  |
| 1445 | 18.3 |  |  |  |  |  |  |
| 1446 | 18.5 |  |  |  |  |  |  |
| 1447 | 17.9 |  |  |  |  |  |  |
| 1448 | 15 |  |  |  |  |  |  |
| 1449 | 9.9 |  |  |  |  |  |  |
| 1450 | 4.6 |  |  |  |  |  |  |
| 1451 | 1.2 |  |  |  |  |  |  |
| 1452 | 0 |  |  |  |  |  |  |
| 1453 | 0 |  |  |  |  |  |  |
| 1454 | 0 |  |  |  |  |  |  |
| 1455 | 0 |  |  |  |  |  |  |

Table A/12
WLTC, Class 3 vehicles, phase Extra High

| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1478 | 0 | 1525 | 72.5 | 1572 | 120.7 | 1619 | 113 |
| 1479 | 2.2 | 1526 | 70.8 | 1573 | 121.8 | 1620 | 114.1 |
| 1480 | 4.4 | 1527 | 68.6 | 1574 | 122.6 | 1621 | 115.1 |
| 1481 | 6.3 | 1528 | 66.2 | 1575 | 123.2 | 1622 | 115.9 |
| 1482 | 7.9 | 1529 | 64 | 1576 | 123.6 | 1623 | 116.5 |
| 1483 | 9.2 | 1530 | 62.2 | 1577 | 123.7 | 1624 | 116.7 |
| 1484 | 10.4 | 1531 | 60.9 | 1578 | 123.6 | 1625 | 116.6 |
| 1485 | 11.5 | 1532 | 60.2 | 1579 | 123.3 | 1626 | 116.2 |
| 1486 | 12.9 | 1533 | 60 | 1580 | 123 | 1627 | 115.2 |
| 1487 | 14.7 | 1534 | 60.4 | 1581 | 122.5 | 1628 | 113.8 |
| 1488 | 17 | 1535 | 61.4 | 1582 | 122.1 | 1629 | 112 |
| 1489 | 19.8 | 1536 | 63.2 | 1583 | 121.5 | 1630 | 110.1 |
| 1490 | 23.1 | 1537 | 65.6 | 1584 | 120.8 | 1631 | 108.3 |
| 1491 | 26.7 | 1538 | 68.4 | 1585 | 120 | 1632 | 107 |
| 1492 | 30.5 | 1539 | 71.6 | 1586 | 119.1 | 1633 | 106.1 |
| 1493 | 34.1 | 1540 | 74.9 | 1587 | 118.1 | 1634 | 105.8 |
| 1494 | 37.5 | 1541 | 78.4 | 1588 | 117.1 | 1635 | 105.7 |
| 1495 | 40.6 | 1542 | 81.8 | 1589 | 116.2 | 1636 | 105.7 |
| 1496 | 43.3 | 1543 | 84.9 | 1590 | 115.5 | 1637 | 105.6 |
| 1497 | 45.7 | 1544 | 87.4 | 1591 | 114.9 | 1638 | 105.3 |
| 1498 | 47.7 | 1545 | 89 | 1592 | 114.5 | 1639 | 104.9 |
| 1499 | 49.3 | 1546 | 90 | 1593 | 114.1 | 1640 | 104.4 |
| 1500 | 50.5 | 1547 | 90.6 | 1594 | 113.9 | 1641 | 104 |
| 1501 | 51.3 | 1548 | 91 | 1595 | 113.7 | 1642 | 103.8 |
| 1502 | 52.1 | 1549 | 91.5 | 1596 | 113.3 | 1643 | 103.9 |
| 1503 | 52.7 | 1550 | 92 | 1597 | 112.9 | 1644 | 104.4 |
| 1504 | 53.4 | 1551 | 92.7 | 1598 | 112.2 | 1645 | 105.1 |
| 1505 | 54 | 1552 | 93.4 | 1599 | 111.4 | 1646 | 106.1 |
| 1506 | 54.5 | 1553 | 94.2 | 1600 | 110.5 | 1647 | 107.2 |
| 1507 | 55 | 1554 | 94.9 | 1601 | 109.5 | 1648 | 108.5 |
| 1508 | 55.6 | 1555 | 95.7 | 1602 | 108.5 | 1649 | 109.9 |
| 1509 | 56.3 | 1556 | 96.6 | 1603 | 107.7 | 1650 | 111.3 |
| 1510 | 57.2 | 1557 | 97.7 | 1604 | 107.1 | 1651 | 112.7 |
| 1511 | 58.5 | 1558 | 98.9 | 1605 | 106.6 | 1652 | 113.9 |
| 1512 | 60.2 | 1559 | 100.4 | 1606 | 106.4 | 1653 | 115 |
| 1513 | 62.3 | 1560 | 102 | 1607 | 106.2 | 1654 | 116 |
| 1514 | 64.7 | 1561 | 103.6 | 1608 | 106.2 | 1655 | 116.8 |
| 1515 | 67.1 | 1562 | 105.2 | 1609 | 106.2 | 1656 | 117.6 |
| 1516 | 69.2 | 1563 | 106.8 | 1610 | 106.4 | 1657 | 118.4 |
| 1517 | 70.7 | 1564 | 108.5 | 1611 | 106.5 | 1658 | 119.2 |
| 1518 | 71.9 | 1565 | 110.2 | 1612 | 106.8 | 1659 | 120 |
| 1519 | 72.7 | 1566 | 111.9 | 1613 | 107.2 | 1660 | 120.8 |
| 1520 | 73.4 | 1567 | 113.7 | 1614 | 107.8 | 1661 | 121.6 |
| 1521 | 73.8 | 1568 | 115.3 | 1615 | 108.5 | 1662 | 122.3 |
| 1522 | 74.1 | 1569 | 116.8 | 1616 | 109.4 | 1663 | 123.1 |
| 1523 | 74 | 1570 | 118.2 | 1617 | 110.5 | 1664 | 123.8 |
| 1524 | 73.6 | 1571 | 119.5 | 1618 | 111.7 | 1665 | 124.4 |


| Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ | Time in s | speed in $\mathrm{km} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1666 | 125 | 1715 | 127.7 | 1764 | 82 |  |  |
| 1667 | 125.4 | 1716 | 128.1 | 1765 | 81.3 |  |  |
| 1668 | 125.8 | 1717 | 128.5 | 1766 | 80.4 |  |  |
| 1669 | 126.1 | 1718 | 129 | 1767 | 79.1 |  |  |
| 1670 | 126.4 | 1719 | 129.5 | 1768 | 77.4 |  |  |
| 1671 | 126.6 | 1720 | 130.1 | 1769 | 75.1 |  |  |
| 1672 | 126.7 | 1721 | 130.6 | 1770 | 72.3 |  |  |
| 1673 | 126.8 | 1722 | 131 | 1771 | 69.1 |  |  |
| 1674 | 126.9 | 1723 | 131.2 | 1772 | 65.9 |  |  |
| 1675 | 126.9 | 1724 | 131.3 | 1773 | 62.7 |  |  |
| 1676 | 126.9 | 1725 | 131.2 | 1774 | 59.7 |  |  |
| 1677 | 126.8 | 1726 | 130.7 | 1775 | 57 |  |  |
| 1678 | 126.6 | 1727 | 129.8 | 1776 | 54.6 |  |  |
| 1679 | 126.3 | 1728 | 128.4 | 1777 | 52.2 |  |  |
| 1680 | 126 | 1729 | 126.5 | 1778 | 49.7 |  |  |
| 1681 | 125.7 | 1730 | 124.1 | 1779 | 46.8 |  |  |
| 1682 | 125.6 | 1731 | 121.6 | 1780 | 43.5 |  |  |
| 1683 | 125.6 | 1732 | 119 | 1781 | 39.9 |  |  |
| 1684 | 125.8 | 1733 | 116.5 | 1782 | 36.4 |  |  |
| 1685 | 126.2 | 1734 | 114.1 | 1783 | 33.2 |  |  |
| 1686 | 126.6 | 1735 | 111.8 | 1784 | 30.5 |  |  |
| 1687 | 127 | 1736 | 109.5 | 1785 | 28.3 |  |  |
| 1688 | 127.4 | 1737 | 107.1 | 1786 | 26.3 |  |  |
| 1689 | 127.6 | 1738 | 104.8 | 1787 | 24.4 |  |  |
| 1690 | 127.8 | 1739 | 102.5 | 1788 | 22.5 |  |  |
| 1691 | 127.9 | 1740 | 100.4 | 1789 | 20.5 |  |  |
| 1692 | 128 | 1741 | 98.6 | 1790 | 18.2 |  |  |
| 1693 | 128.1 | 1742 | 97.2 | 1791 | 15.5 |  |  |
| 1694 | 128.2 | 1743 | 95.9 | 1792 | 12.3 |  |  |
| 1695 | 128.3 | 1744 | 94.8 | 1793 | 8.7 |  |  |
| 1696 | 128.4 | 1745 | 93.8 | 1794 | 5.2 |  |  |
| 1697 | 128.5 | 1746 | 92.8 | 1795 | 0 |  |  |
| 1698 | 128.6 | 1747 | 91.8 | 1796 | 0 |  |  |
| 1699 | 128.6 | 1748 | 91 | 1797 | 0 |  |  |
| 1700 | 128.5 | 1749 | 90.2 | 1798 | 0 |  |  |
| 1701 | 128.3 | 1750 | 89.6 | 1799 | 0 |  |  |
| 1702 | 128.1 | 1751 | 89.1 | 1800 | 0 |  |  |
| 1703 | 127.9 | 1752 | 88.6 |  |  |  |  |
| 1704 | 127.6 | 1753 | 88.1 |  |  |  |  |
| 1705 | 127.4 | 1754 | 87.6 |  |  |  |  |
| 1706 | 127.2 | 1755 | 87.1 |  |  |  |  |
| 1707 | 127 | 1756 | 86.6 |  |  |  |  |
| 1708 | 126.9 | 1757 | 86.1 |  |  |  |  |
| 1709 | 126.8 | 1758 | 85.5 |  |  |  |  |
| 1710 | 126.7 | 1759 | 85 |  |  |  |  |
| 1711 | 126.8 | 1760 | 84.4 |  |  |  |  |
| 1712 | 126.9 | 1761 | 83.8 |  |  |  |  |
| 1713 | 127.1 | 1762 | 83.2 |  |  |  |  |
| 1714 | 127.4 | 1763 | 82.6 |  |  |  |  |


[^0]:    ${ }^{1}$ UNECE. Vehicle Regulations, Regulation No. 83, http://www.unece.org/trans/main/wp29/wp29regs81-100.html
    ${ }^{2}$ TRIAS 31-J042-01 TEST PROCEDURE FOR EXHAUST EMISSION MEASUREMENT OF LIGHT- AND MEDIUM-DUTY MOTOR VEHICLES (PROCEDURE FOR JC08H+JC08C-MODE)
    ${ }^{3}$ CODE OF FEDERAL REGULATIONS, Title 40, Part 86, Appendix I

[^1]:    ${ }^{4}$ WLTP-DHC-02-06 Draft in-use data collection guidelines

[^2]:    ${ }^{5}$ IBM. Statistical Package for the Social Sciences (SPSS). Available from: http://www-01.ibm.com/software/analytics/spss/

[^3]:    ${ }^{6}$ WLTP-DHC-02-05 Draft methodology to develop WLTP drive cycle
    ${ }^{7}$ WLTP-DHC-06-03 WLTC methodology

[^4]:    ${ }^{8}$ EU: TREMOVE http://www.tremove.org/, INDIA: WORLD ROAD STSTISTICS 2009 DATA 2002-2007 (http://www.irfnet.org/statistics.php), JAPAN: Road Traffic Census Data 2005 (MLIT), USA: EPA

[^5]:    ${ }^{9}$ Van de Weijer, C., Heavy Duty Emission Factors: Development of Representative Driving Cycles and Prediction of Emissions in Real Life. 1997.

[^6]:    ${ }^{10} \mathrm{http}: / /$ www.unece.org/trans/main/wp29/wp29wgs/wp29grpe/wltp_dhc10.html

[^7]:    ${ }^{11} \mathrm{http}: / /$ www.unece.org/trans/main/wp29/wp29wgs/wp29grpe/wltp_dhc12.html

[^8]:    ${ }^{12} \mathrm{https}: / / \mathrm{www} 2 . u n e c e . o r g /$ wiki/download/attachments/5801079/WLTP-DHC-16-06e_rev.xlsx

[^9]:    ${ }^{13} \mathrm{https}: / / \mathrm{www} 2 . \mathrm{unece}$. org/wiki/download/attachments/5801079/WLTP-DHC-16-06e_rev.xlsx

[^10]:    ${ }^{14} \mathrm{https}: / / \mathrm{www} 2 . \mathrm{unece}$. org/wiki/download/attachments/5801079/WLTP-DHC-16-06e_rev.xlsx

